

# **Fundamentals of Radiation Damage: Fun with Vacancies and Interstitials**

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**ATR NSUF Summer School  
Fuels and Materials Course**

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**The primary objective of this talk is to explore the basics of radiation damage and basic effects.**

## **Outline**

- **Introduction to Radiation Damage**
- **The “5-scourges of radiation damage!”**
  - **Diffusion-related radiation degradation**
  - **Clustering-related radiation degradation**
- **Other forms of degradation**



# **What should you expect to take away from this lecture?**

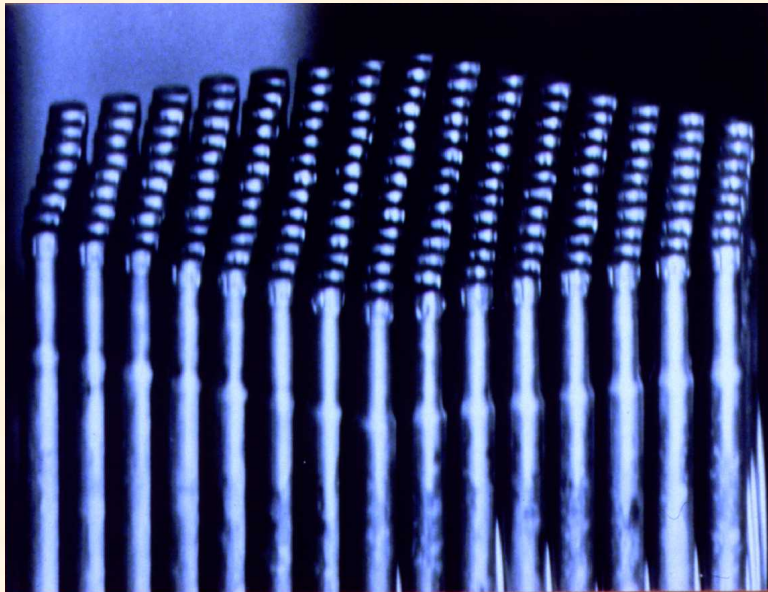
- **Basic understanding of neutron interactions with crystalline materials**
- **An appreciation for the exciting lives of vacancies and interstitials**
- **A survey of modes of degradation common to LWR and fast reactors**
- **No equations**

# **Fundamentals of Radiation Damage**

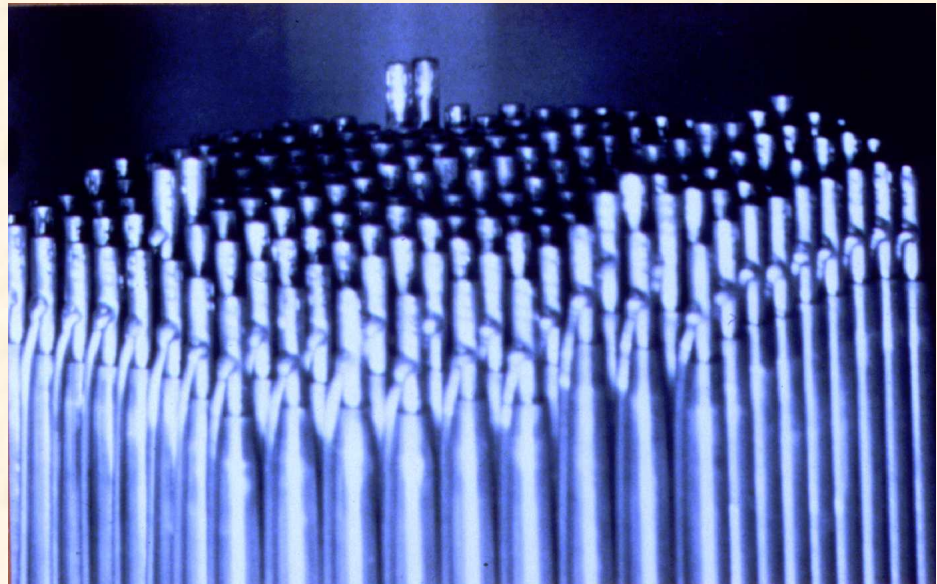
**Motivation: Why do we care about radiation damage?**

# Swelling can create tolerance problems

## FFTF Fuel Pin Bundles



**HT-9, no swelling**



**316-Ti stainless, swelling**

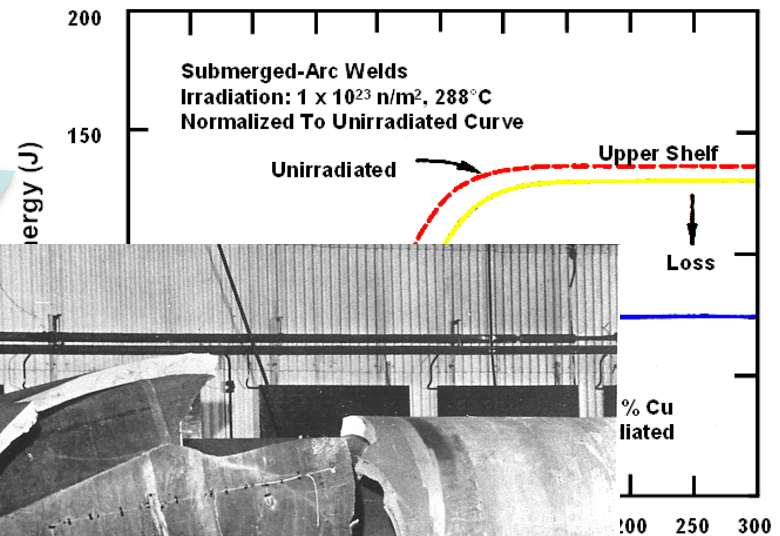
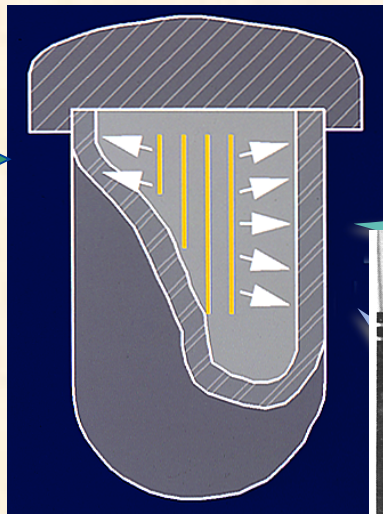
*Source: F. Garner*



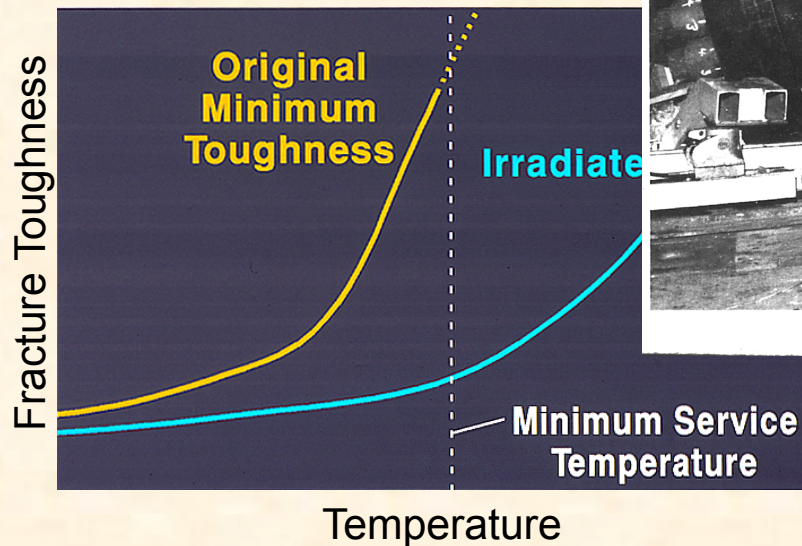
# Reactor Vessel Integrity Experiences Potential Degrading Effects of Neutron Irradiation

Irradiation Causes Ductile/Brittle Transition Temperature Shift and Upper Shelf Energy Loss  
— Copper Increases The Effect

Neutron  
Embrittlement  
of RPV



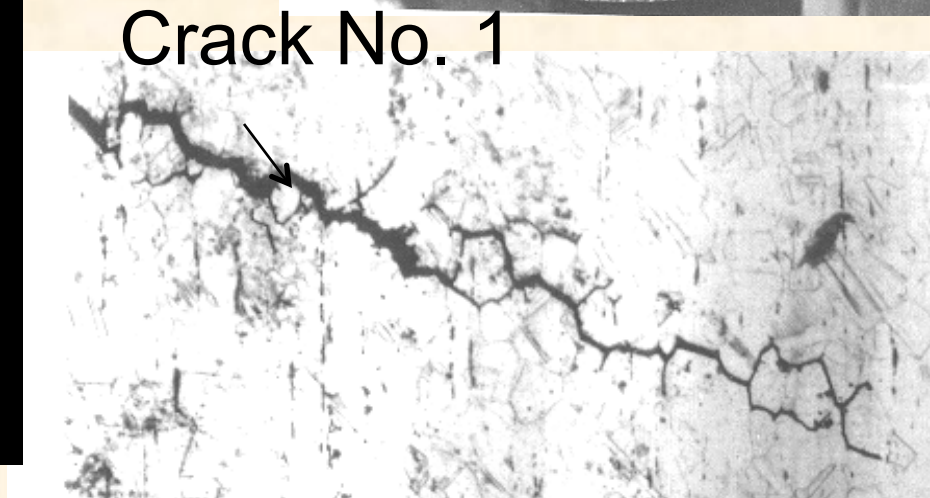
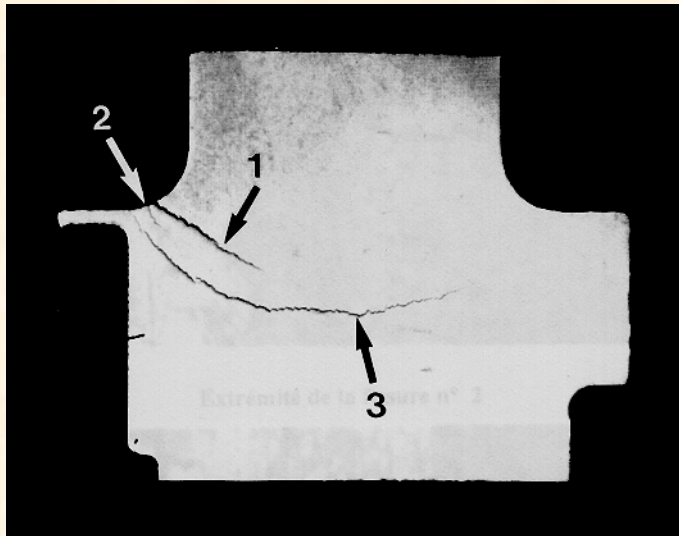
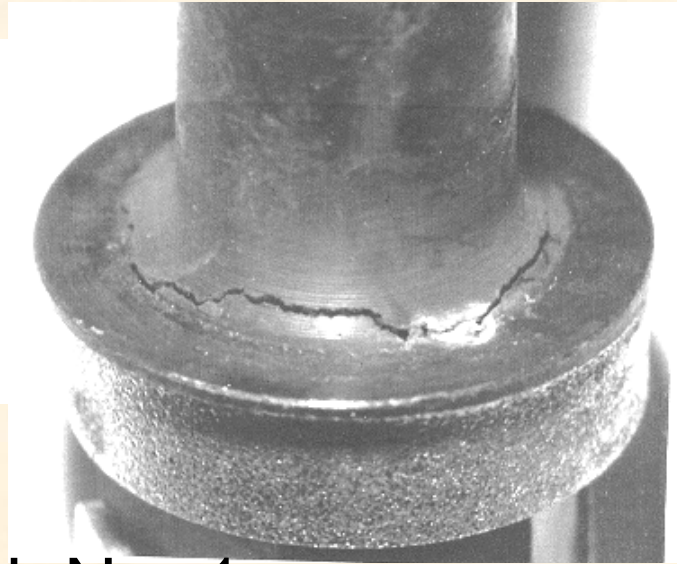
CATASTROPHIC FAILURE OF PRESSURE VESSEL DURING HYDROSTATIC TESTING; DUE TO IMPROPER POSTWELD HEAT TREATMENT



and  
structures:  
precipitates and  
Matrix Damage

Source: R. Nanstad

# IASCC affects baffle former bolts in PWRs



Source: G.S. Was

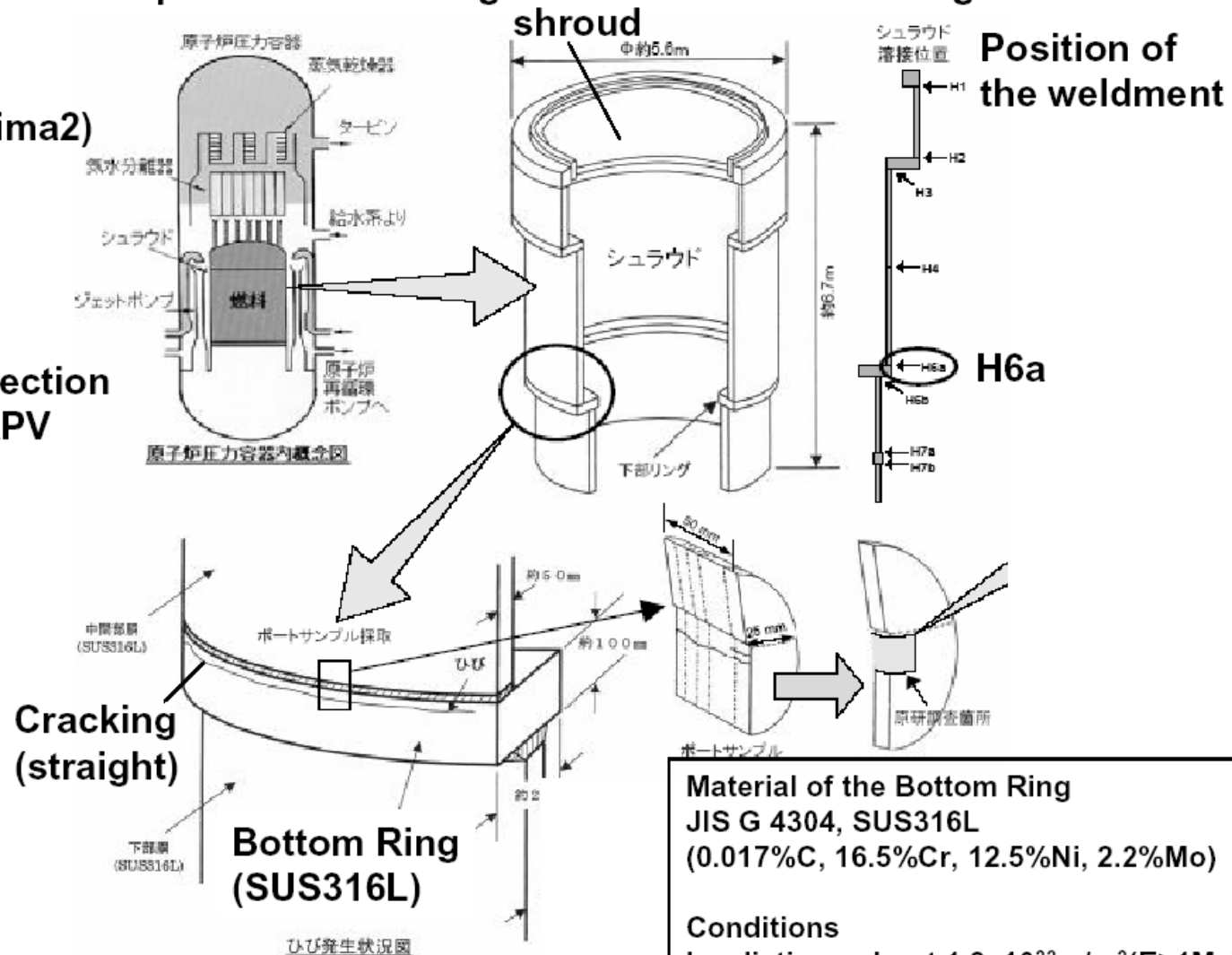


### 3. Research ~Examples of the Investigation Results for Cracking~

#### 3.1 Shroud

(Unit3  
-Fukushima2)

Cross section  
of the RPV

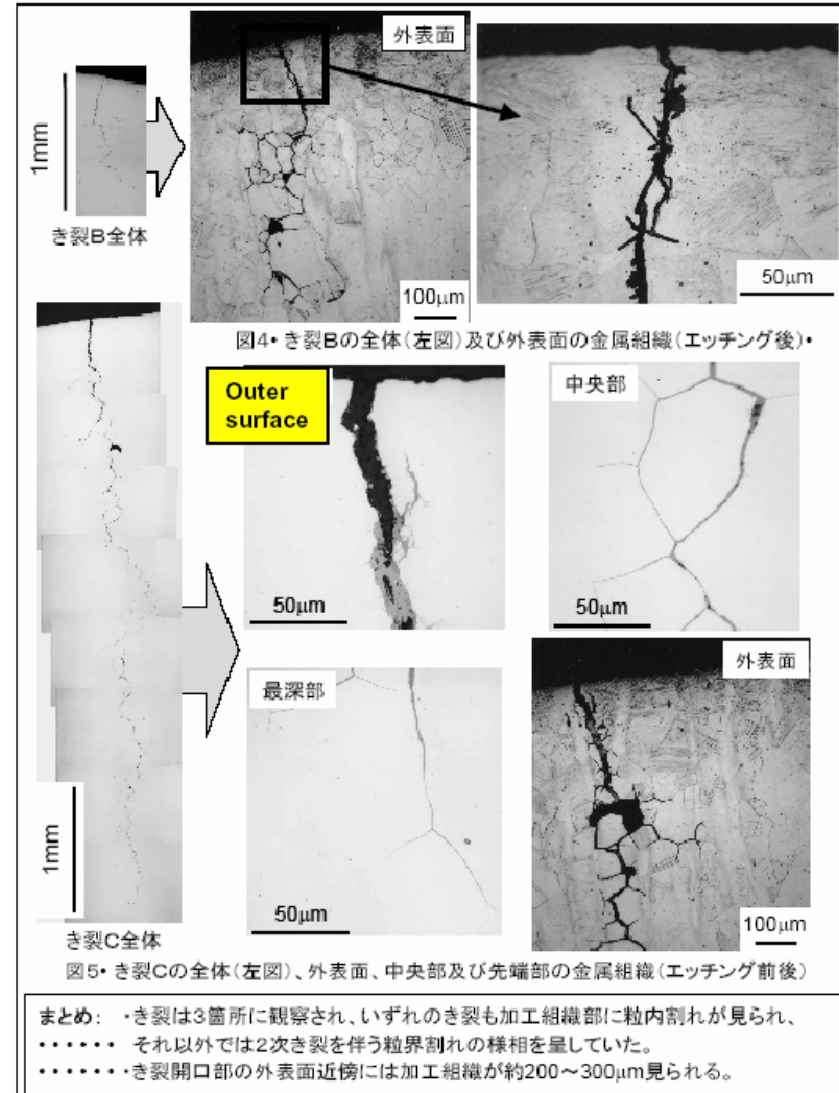
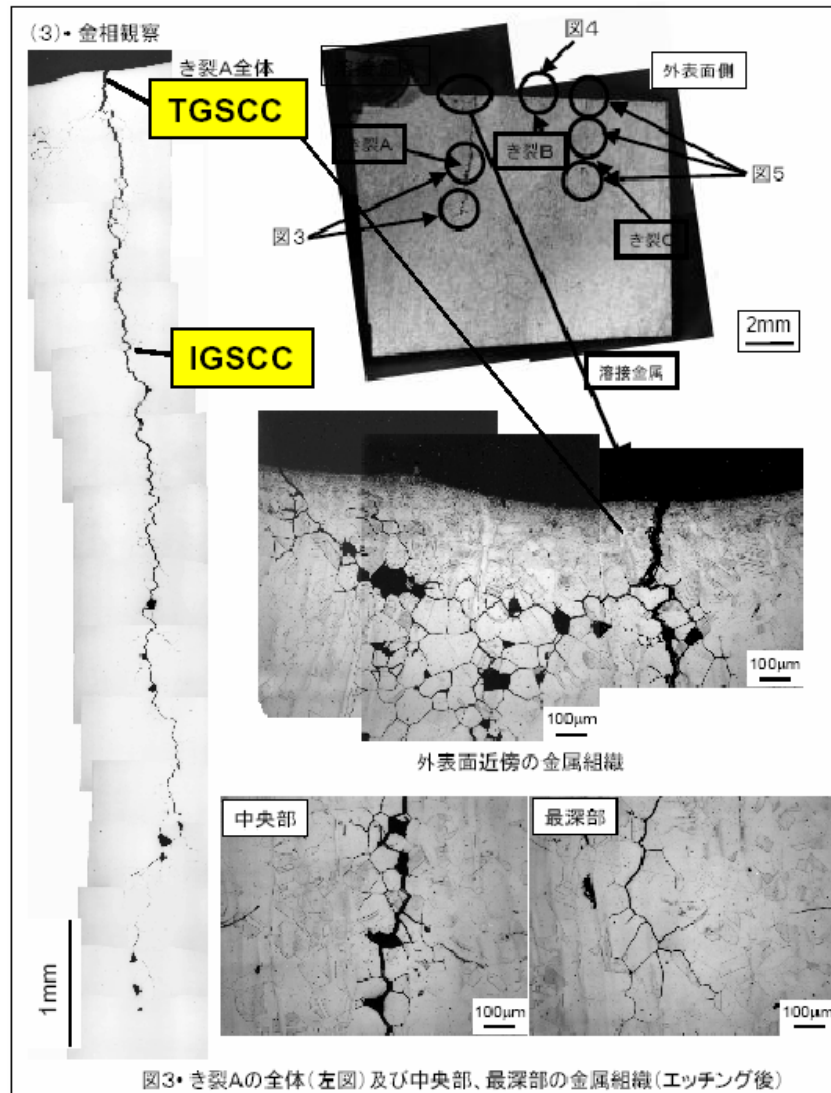


**Material of the Bottom Ring**  
JIS G 4304, SUS316L  
(0.017%C, 16.5%Cr, 12.5%Ni, 2.2%Mo)

**Conditions**  
Irradiation : about  $1.3 \times 10^{22}$  n/m<sup>2</sup> (E>1MeV)  
Temperature : about 288 deg.  
Dissolved Oxygen : about 250 ppb

Source: G.S. Was

## Cracking of the Shroud (2F-3) ~ Microscopic observation ~

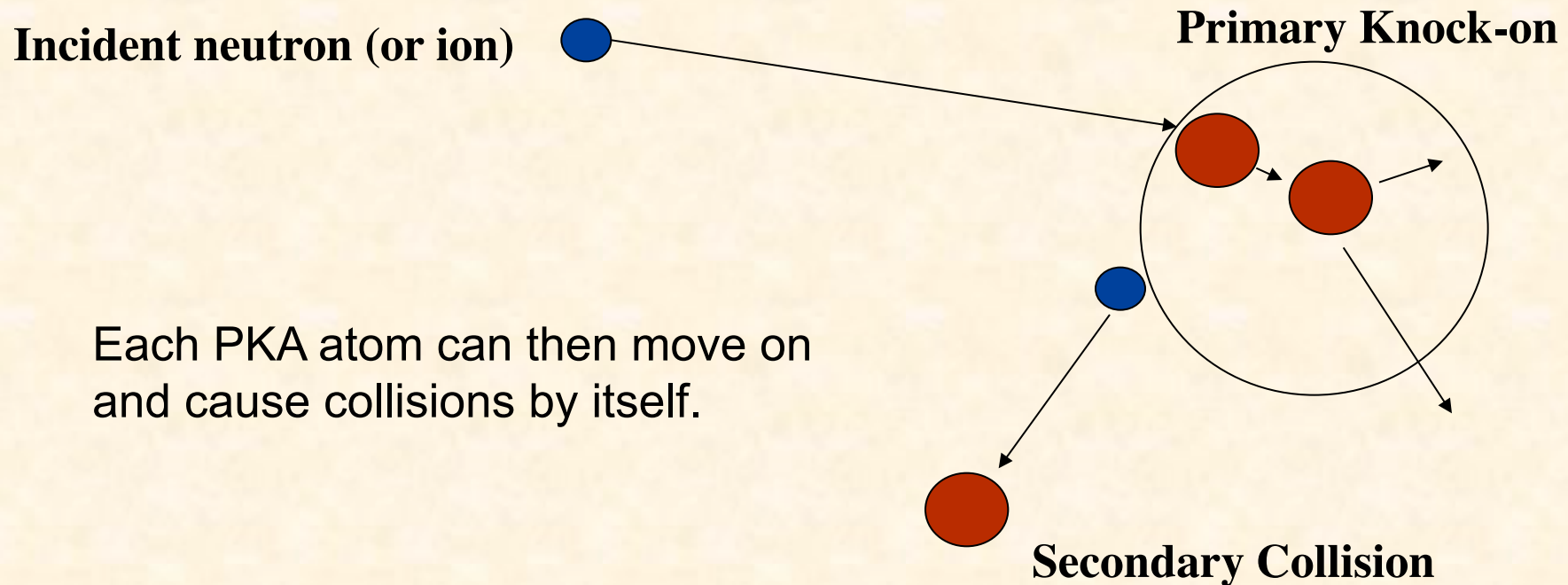


# **Fundamentals of Radiation Damage**

## **The basics**

# Radiation Damage: the basics

- All of radiation damage boils down to a common step: **collisions between incoming neutrons and atoms in the crystal lattice!**

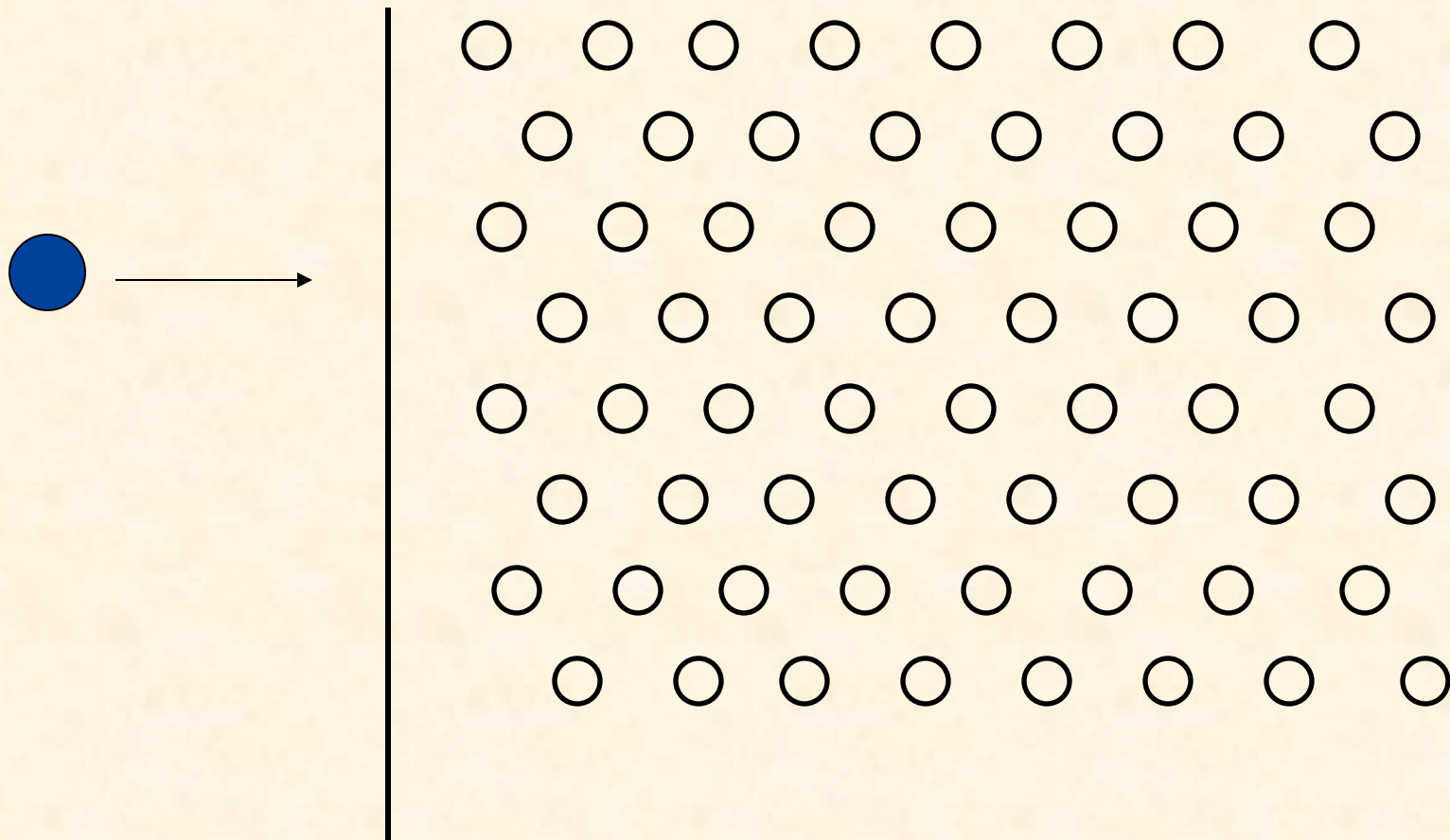


# **Primary Knockon Atoms are an important part of the damage process**

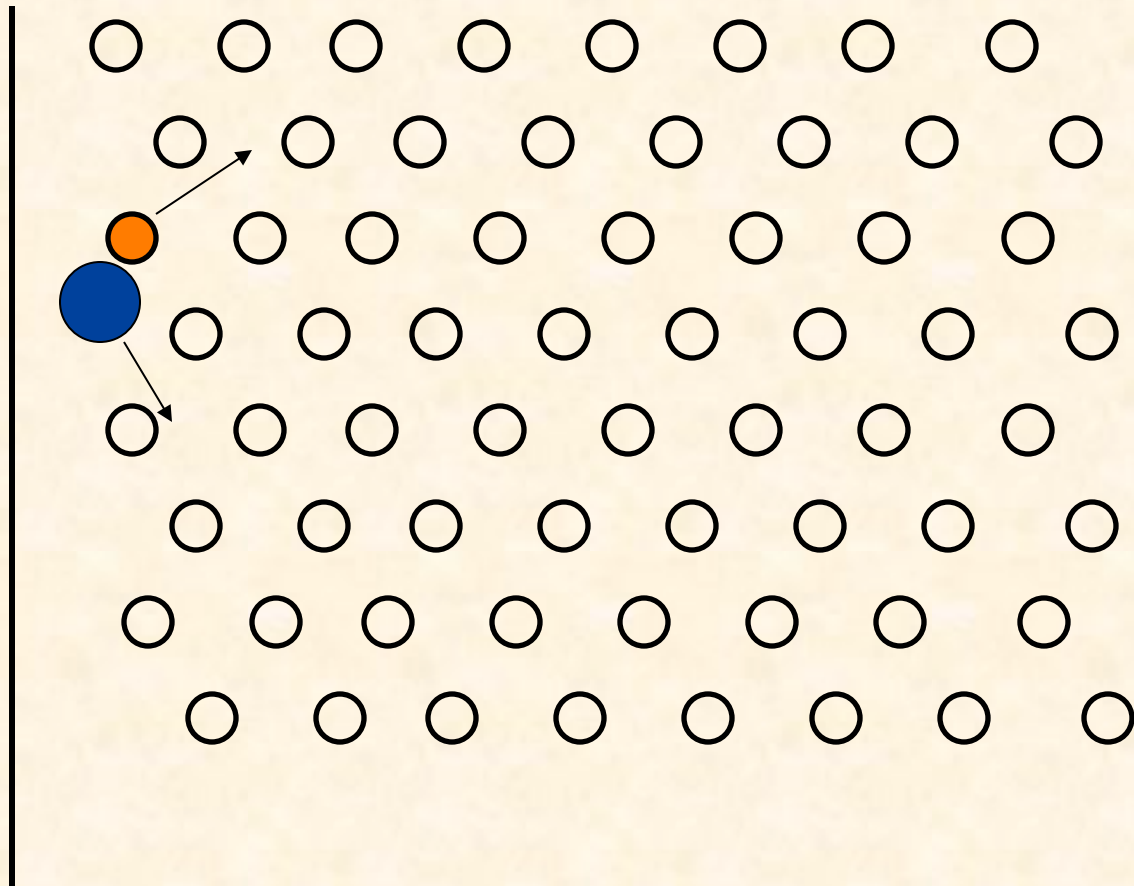
- **Each neutron/atom collision transfers energy. For neutrons, this number varies**
  - **Average kinetic energy for PKA in a fission reactor: 10 keV**
  - **Average kinetic energy for PKA in a fusion reactor: 50 keV**
- **As long as the energy of the PKA is above the energy to displace an atom ( $E_d \sim 40\text{-}50$  eV), each PKA will transfer energy to other atoms in the crystal.**
- **This process continues creating a cascade.**



# Simple Picture

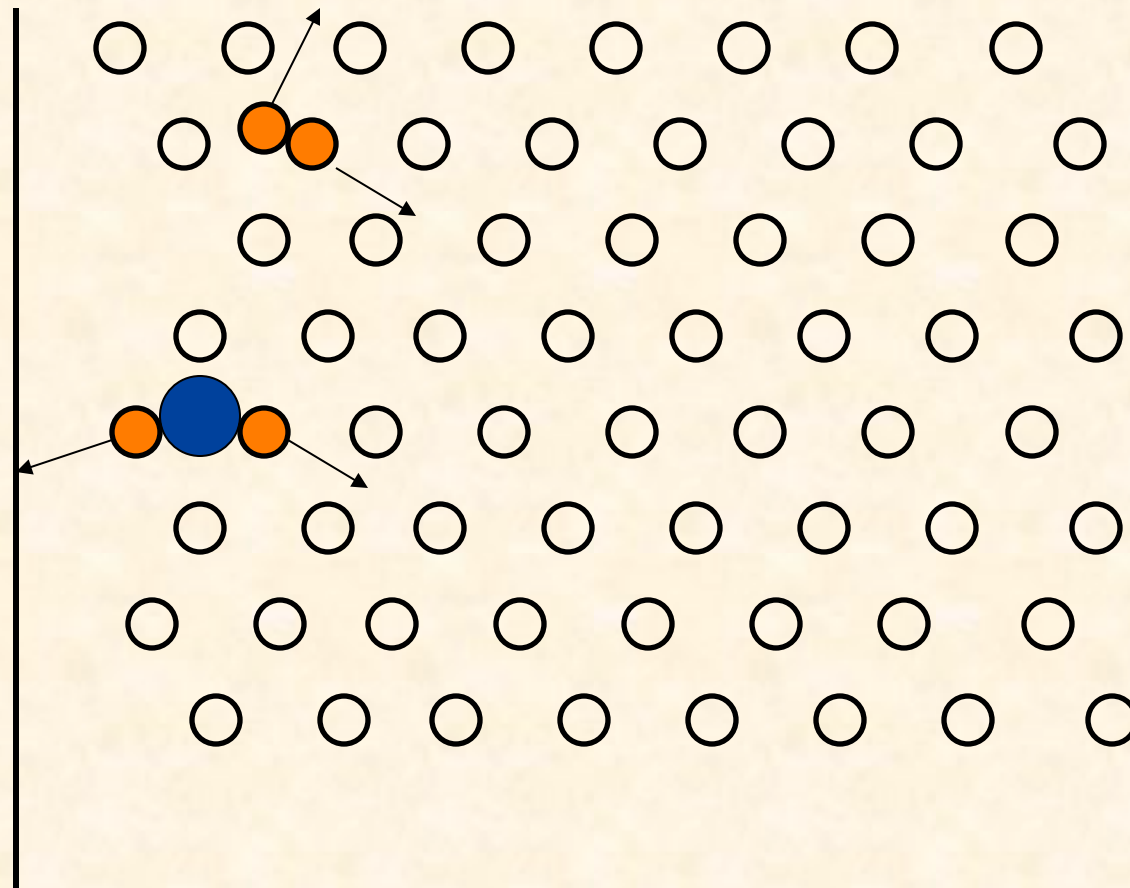


# Simple Picture

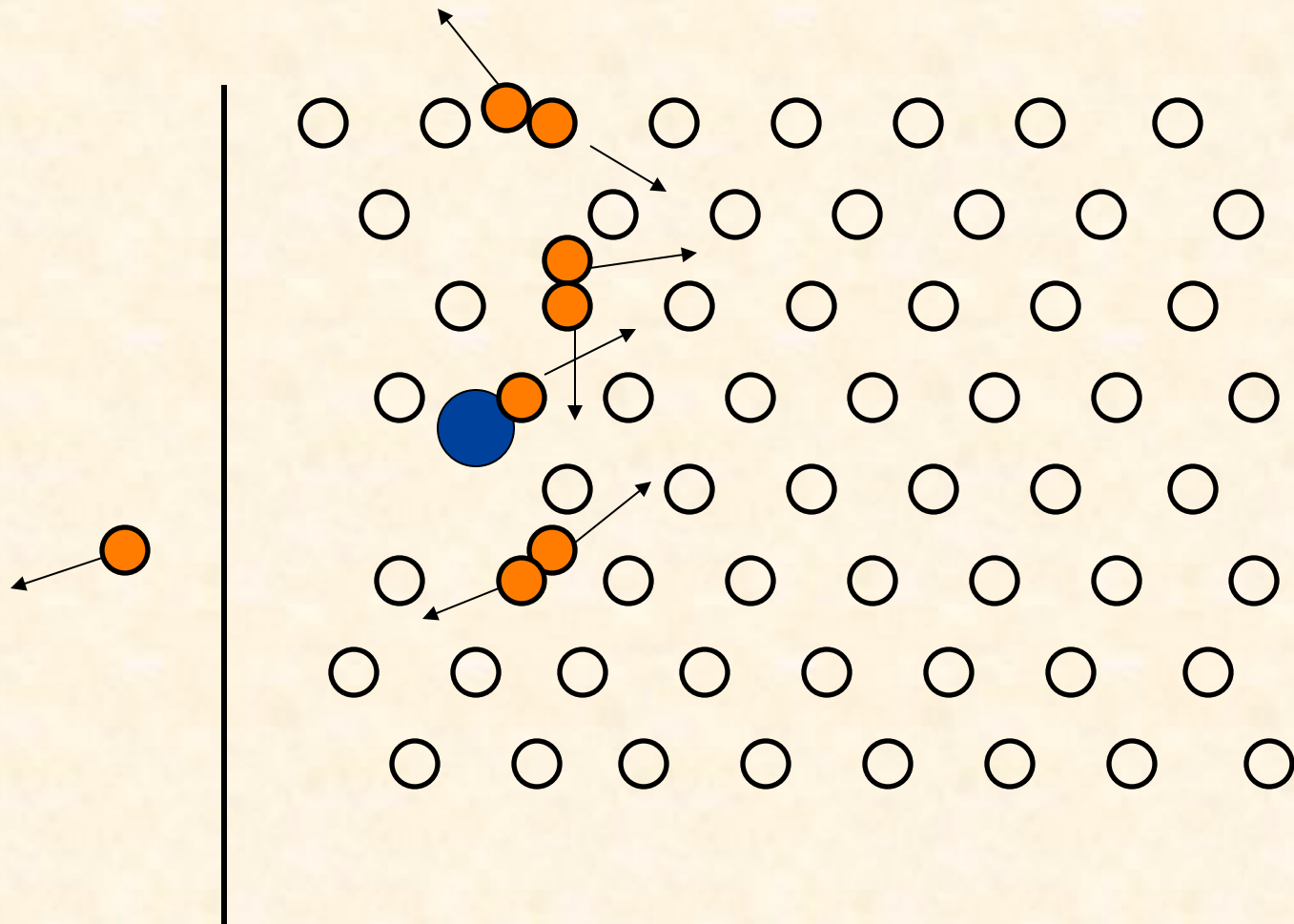


Source: T.R. Allen

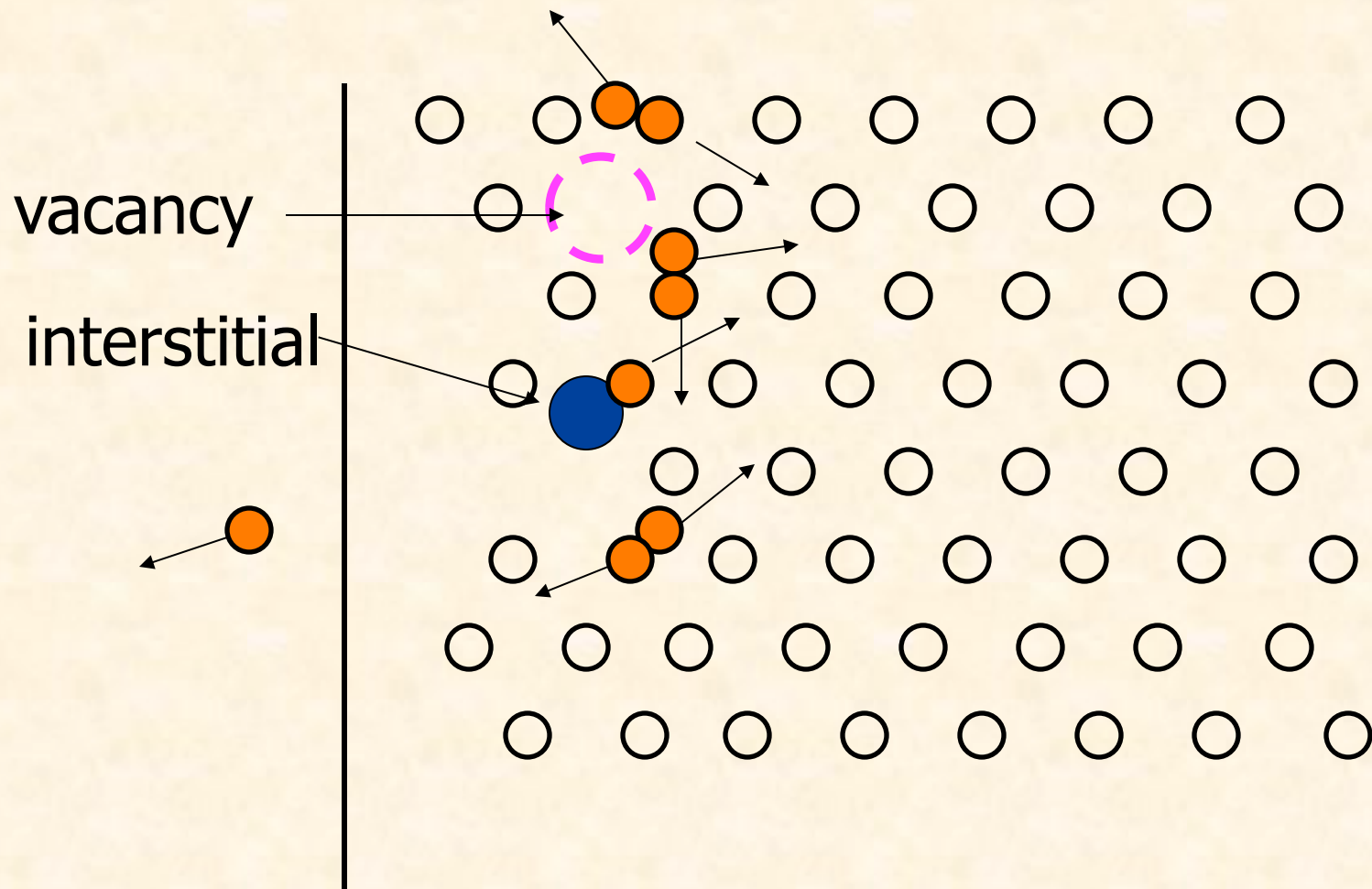
# Simple Picture



# Simple Picture



# Simple Picture





# **Molecular dynamics provides an easier way to visualize cascades**

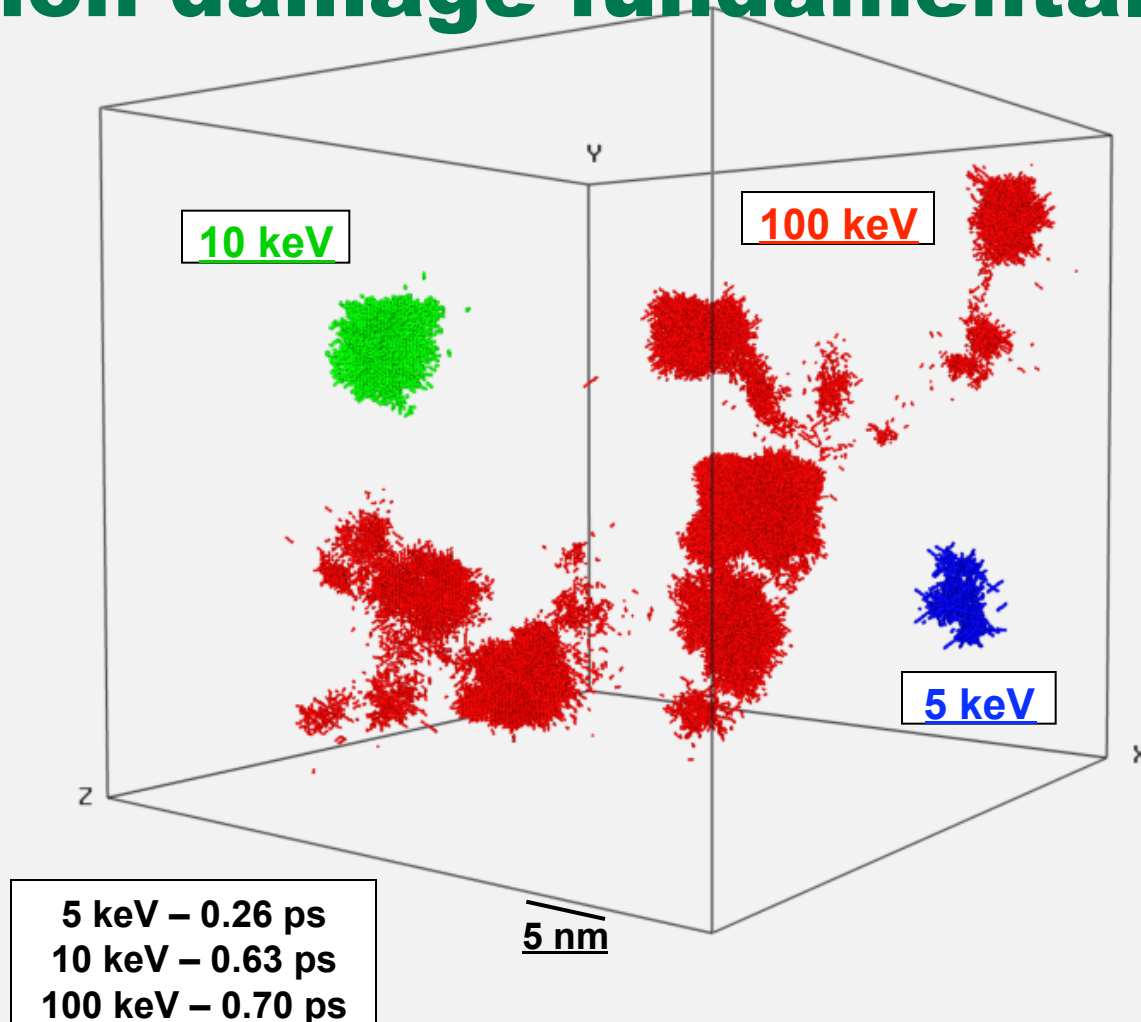
- **While we can't directly observe these interactions, we can model them.**
- **Molecular dynamic simulations have been invaluable in learning about these interactions.**

# Molecular dynamic simulations

- MD movie:

*Source: R. Stoller*

# Molecular dynamics have provided considerable information on radiation damage fundamentals



Source: R. Stoller

# Dynamics of a displacement cascade

- The creation and subsequent decay of a displacement cascade consists of three overlapping stages.
  - **Collisional phase**  $\sim 10^{-13}$  s: All of the collisions associated with the PKA occur.
  - **Cooling phase**  $\sim 10^{-11}$  s: Annihilation, in-cascade clustering, replacement events occur.
  - **Diffusional interactions phase**  $> 10^{-11}$  s: Mobile defects interact in the lattice to form clusters or annihilate via recombination or at sinks.
- The total number of atoms displaced by each neutron depends on a number of factors:
  - Incoming particle (energy, direction)
  - Material ( $E_d$ , crystal structure)
  - Temperature

# Ions also create cascades and defects

1 MeV electrons

$T = 60 \text{ eV}$

$\epsilon = 50\text{-}100\%$

1 MeV protons

$T = 200 \text{ eV}$

$\epsilon = 25\%$

1 MeV heavy ions

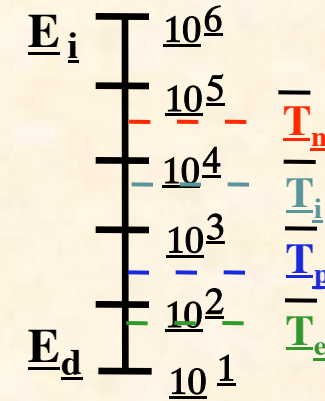
$T = 5 \text{ keV}$

$\epsilon = 4\%$

1 MeV neutrons

$T = 35 \text{ keV}$

$\epsilon = 2\%$



Source: G.S. Was

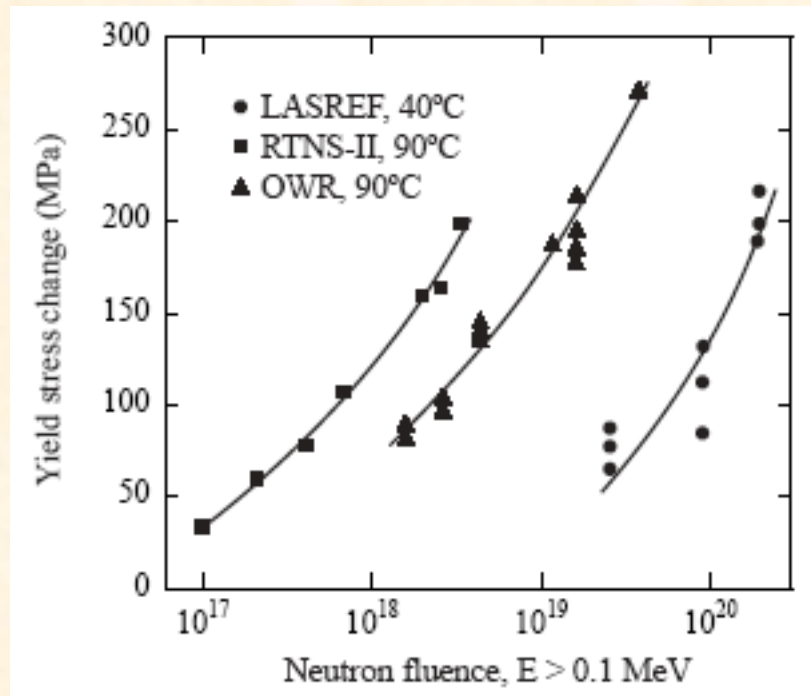


# Damage is often normalized into “displacements per atom”

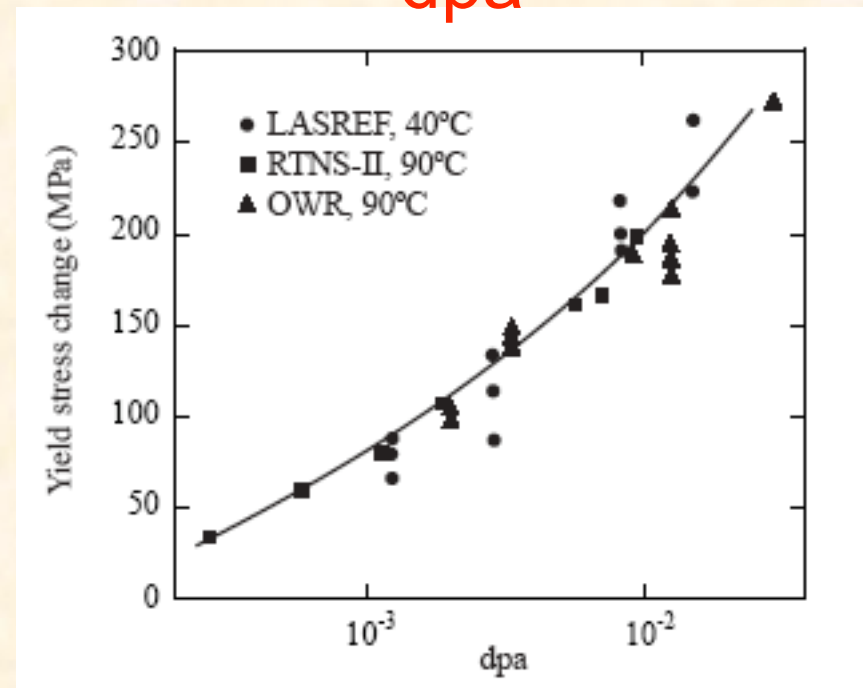
- Displacement per atom (dpa) = average number of displacements of each lattice atom
- This calculated value is convenient as it can help normalize between different neutron spectra or even particles
- Rules of thumb:
  - $0.7 \times 10^{21} \text{ n/cm}^2$  ( $E > 1 \text{ MeV}$ )  $\approx 1 \text{ dpa}$  in SS
  - $0.4 \times 10^{21} \text{ n/cm}^2$  ( $E > 1 \text{ MeV}$ )  $\approx 1 \text{ dpa}$  in Zr
- For a fast reactor core ( $10^{15} \text{ n/cm}^2/\text{s}$ ), displacement rates of  $10^{-6} \text{ dpa/s}$  may be experienced. Each atom is displaced every  $\sim 12$  days.

# Dpa can actually be validated as an accurate measure of damage

Fluence



dpa



Normalizing to DPA works!

*Radiation-induced strengthening of 316 stainless steel in radically different neutron spectra (Heinisch and Martinez, 1986)*

# **Fundamentals of Radiation Damage**

**How can vacancies and interstitials possible cause problems?**





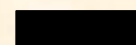


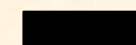

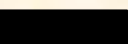





# **Radiation induced defects are produced in very large numbers**

- **Depending on material, temperature, and dose rate, excess vacancies and interstitials can be created at 4-6 orders of magnitude above thermal equilibrium.**
- **Defect populations in excess of equilibrium must be removed!**

# **What happens when a system is far from equilibrium?**

- **That system tries to move back to equilibrium. But how?**
- **Defects can be removed in a number of ways**
  - **Recombination**
  - **Diffusion to surfaces**
  - **Diffusion to particles or precipitates**
  - **Diffusion to grain boundaries**
  - **Cluster together**

# Temperature and dose rate influence populations and their actions

Effect		Thermal Defect Population	Irrad. Defect Population	Diffusion	Typical Leading Process
Constant Dose Rate	Low Temperature				Clustering/ Recomb.
	Moderate Temperature				Diffusion
	High Temperature				Recomb./ Diffusion
Constant Temperature	Decrease Dose Rate				Diffusion/ Clustering
	Increase Dose Rate				Clustering/ Recomb.

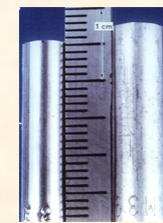
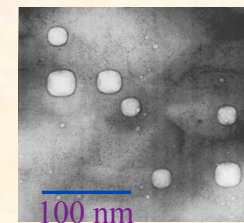
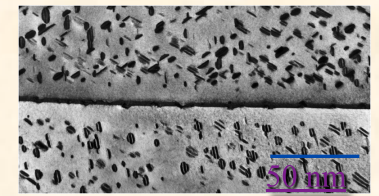
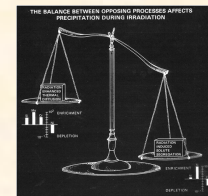
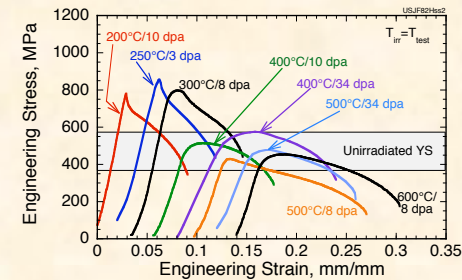
# **Freely migrating defects and their actions are the key to radiation damage**

- **Regardless of the nature of radiation (reactor, spectrum, particle), the surviving defects are the key for long-term material changes and properties**
- **Defects may**
  - **Recombine**
  - **Diffuse**
  - **Cluster**
- **The latter two possibilities will result in distinct changes.**



# Radiation Damage can Produce Large Changes in Structural Materials

- **Radiation hardening and embrittlement** ( $<0.4 T_M$ ,  $>0.1$  dpa)
- **Phase instabilities from radiation-induced precipitation** ( $0.3-0.6 T_M$ ,  $>10$  dpa)
- **Irradiation creep** ( $<0.45 T_M$ ,  $>10$  dpa)
- **Volumetric swelling from void formation** ( $0.3-0.6 T_M$ ,  $>10$  dpa)
- **High temperature He embrittlement** ( $>0.5 T_M$ ,  $>10$  dpa)



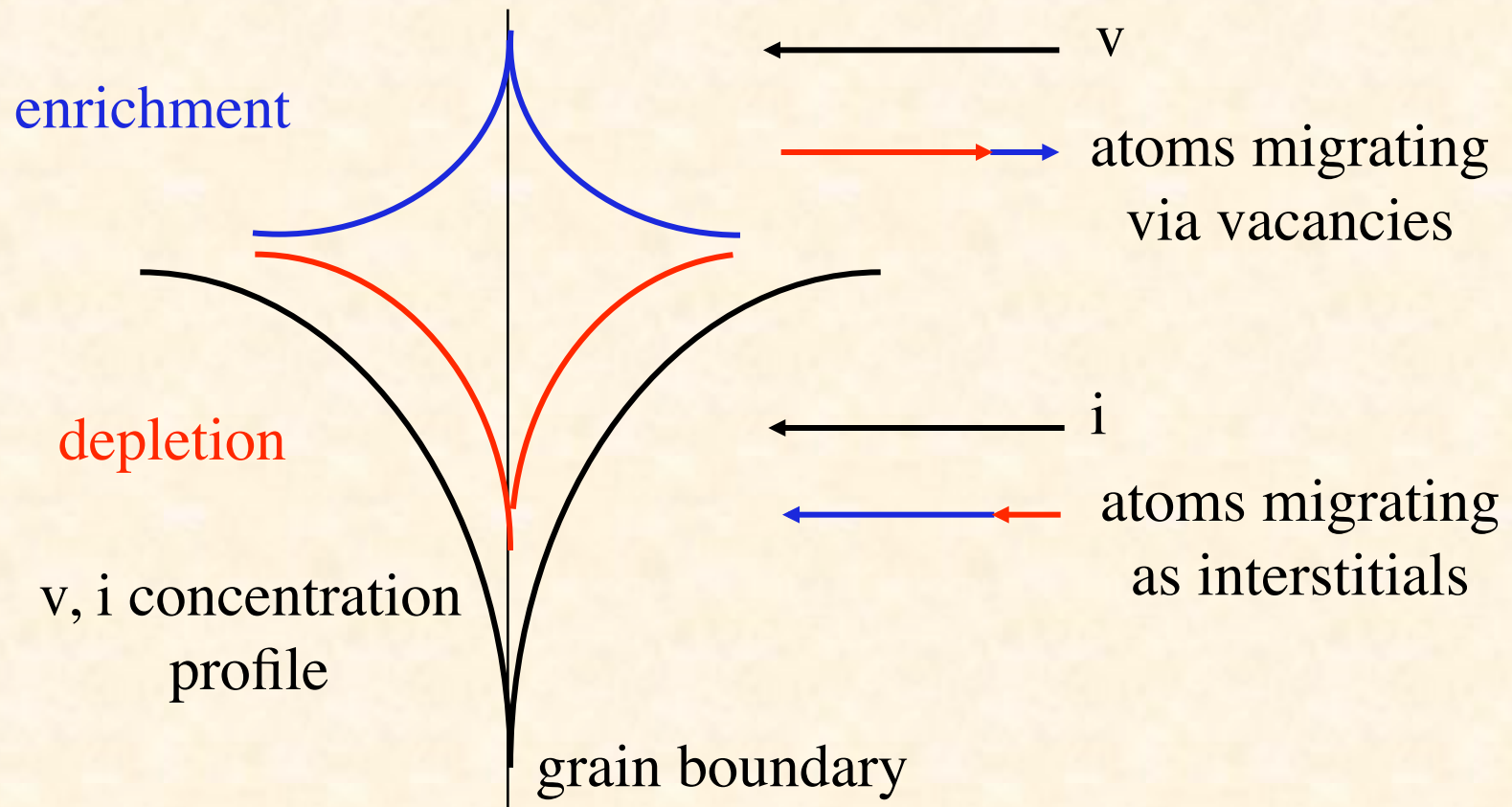
Source: S. Zinkle



# **Fundamentals of Radiation Damage**

## **Diffusion-related forms of radiation-induced degradation**

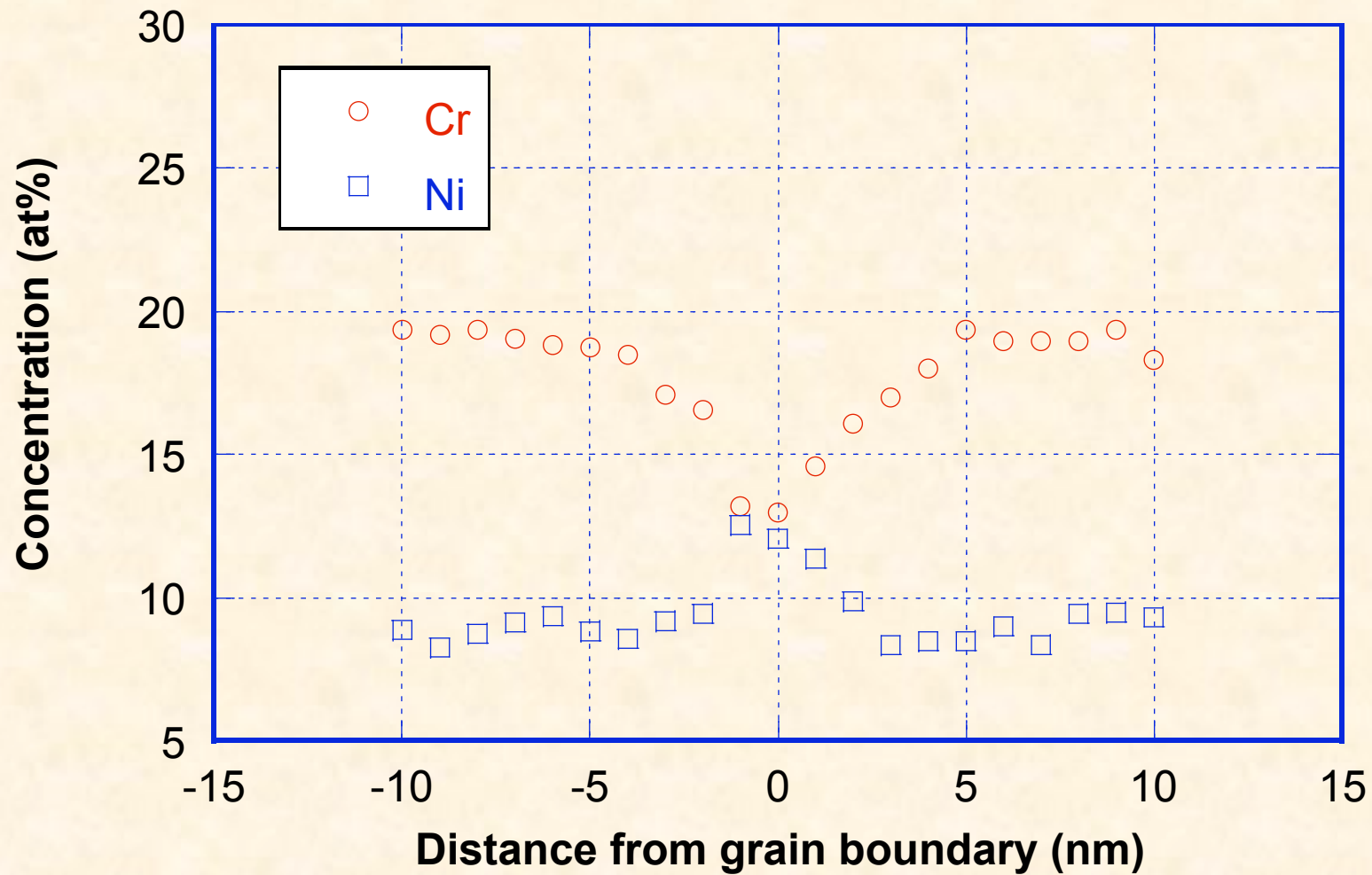
# Radiation-Induced Segregation



- High concentrations of radiation-induced defects will migrate to defect sinks.
- Any preferential association between an atom and one type of defect will result in segregation.

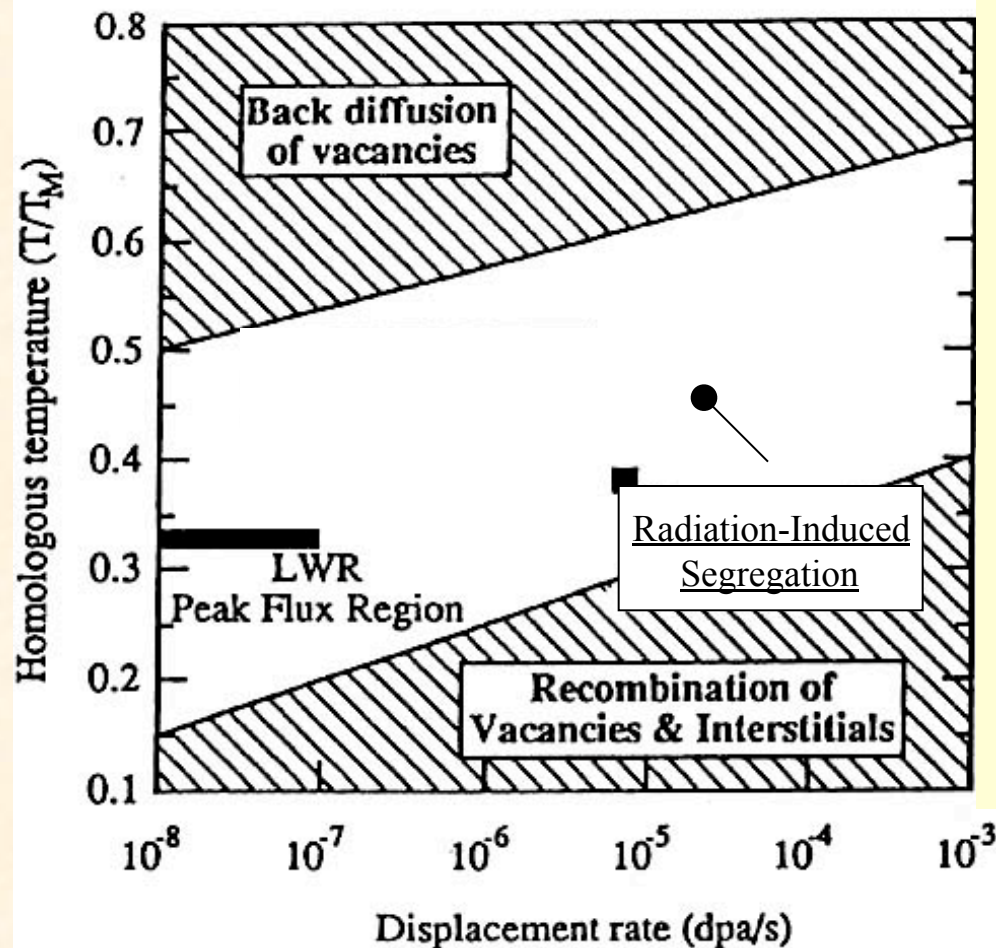
# Grain Boundary Segregation

304 SS, proton irradiated at 400°C to a dose of 1.0 dpa



Source: T.R. Allen<sup>83</sup>

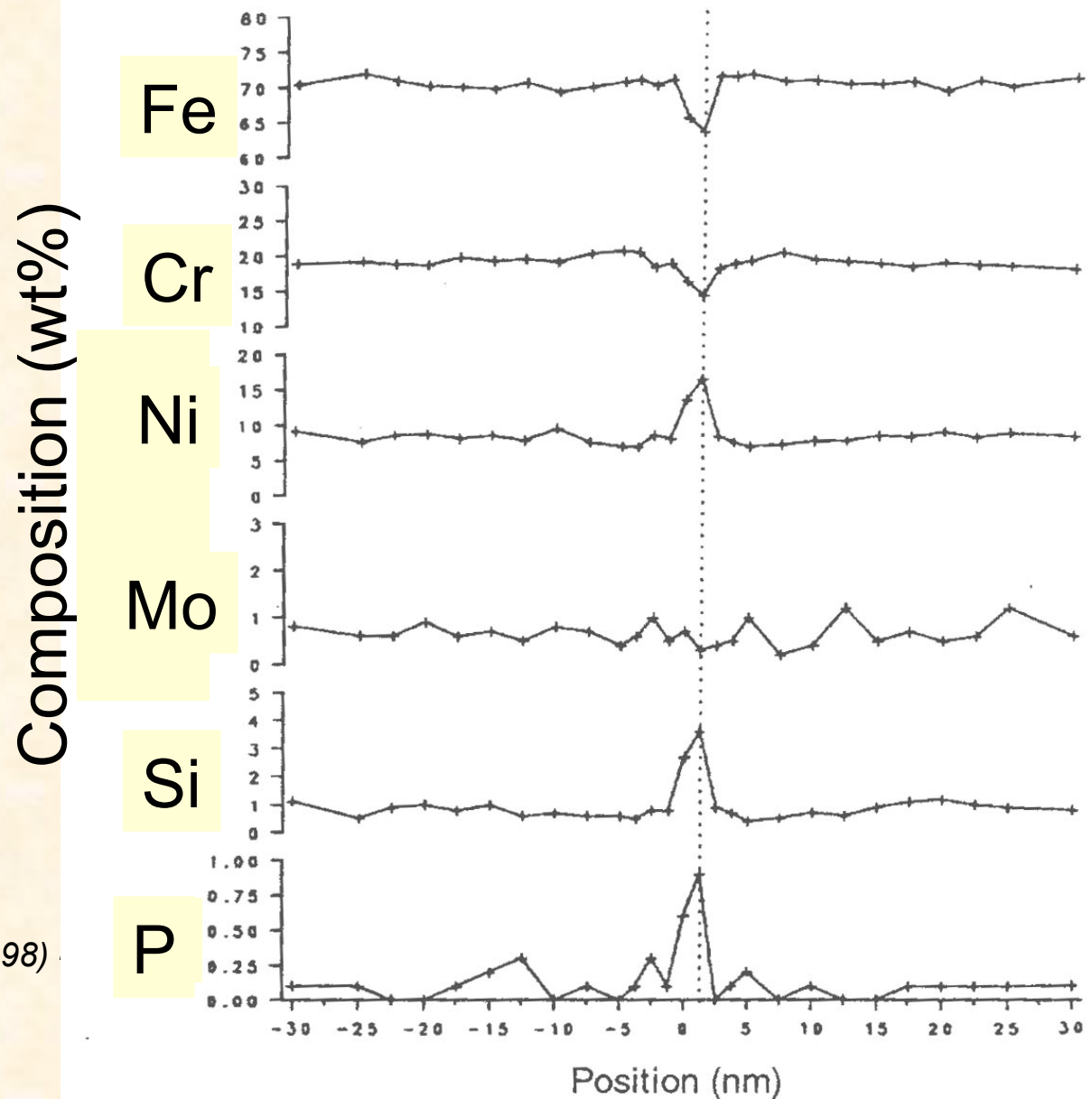
# Radiation-induced segregation depends on temperature and dose rate



- The degree of segregation under irradiation will vary with temperature and dose rate.
- At low temperatures where defect mobility is limited, defect recombination dominates and RIS is minimal.
- At high temperatures where defect mobility and thermally induced defect populations are high, diffusion works to prevent or remove any composition gradients.
- At intermediate temperatures, however, RIS will occur.

# Concentration profiles for CP 304 SS after $\sim 1022 \text{ n/cm}^2$ at $288^\circ\text{C}$

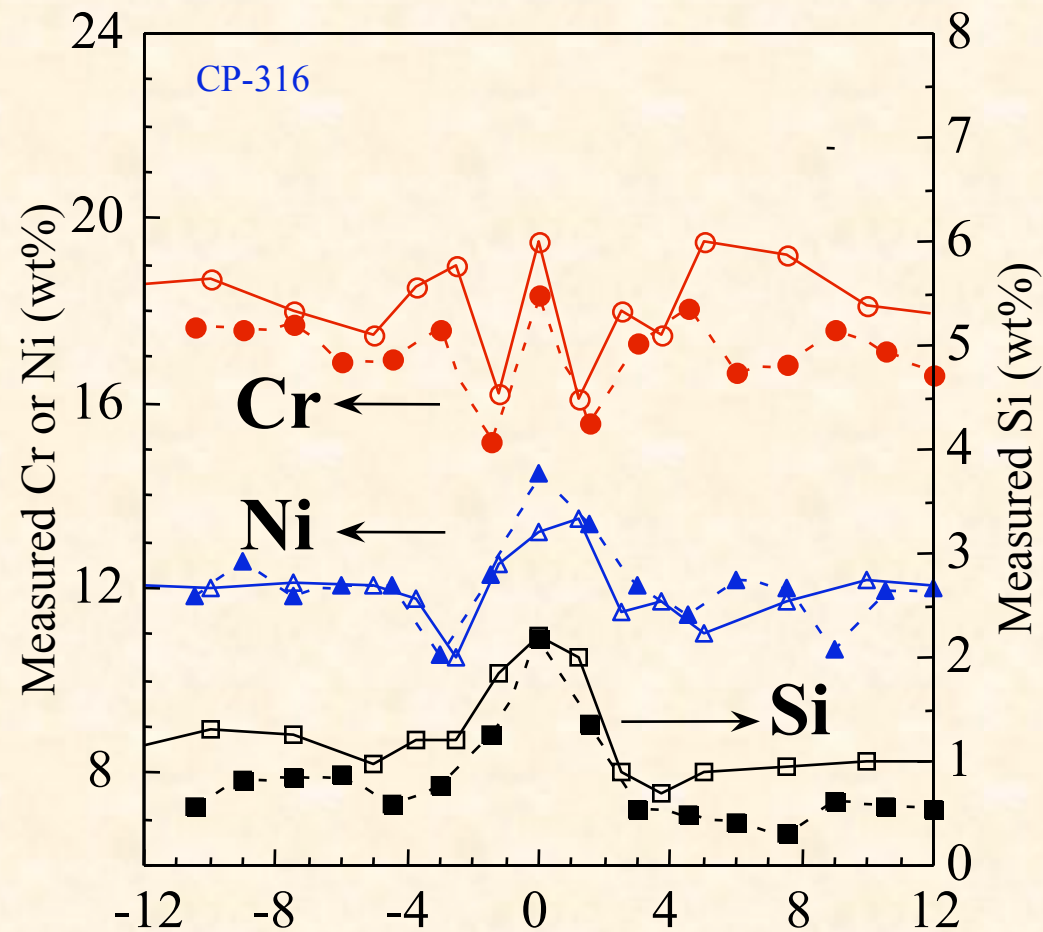
Cr, Mo deplete  
Ni, Si, P enrich  
Fe depends on alloy  
composition



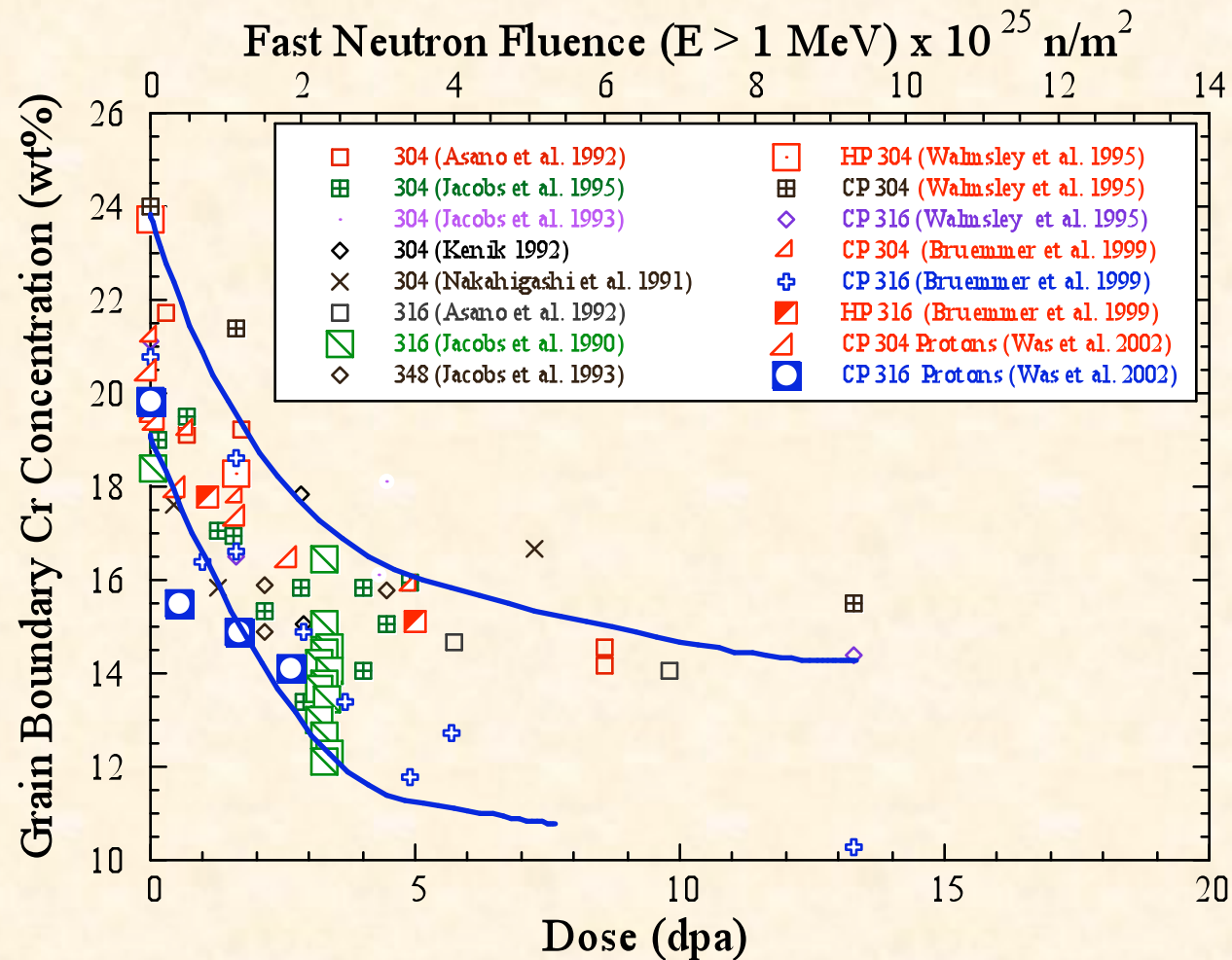
A. Jenssen et al, Corrosion 54 1 (1998)



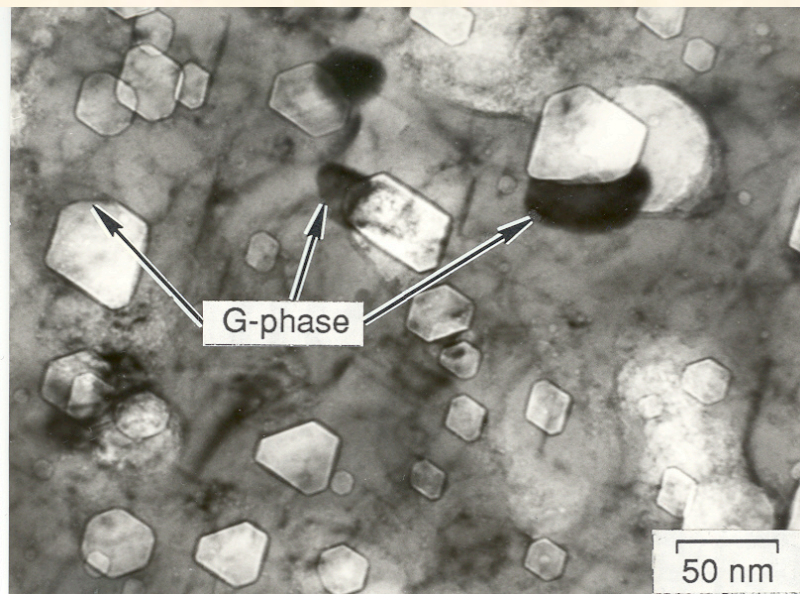
# RIS can be quite complicated



# Grain Boundary Chromium Depletion can be significant

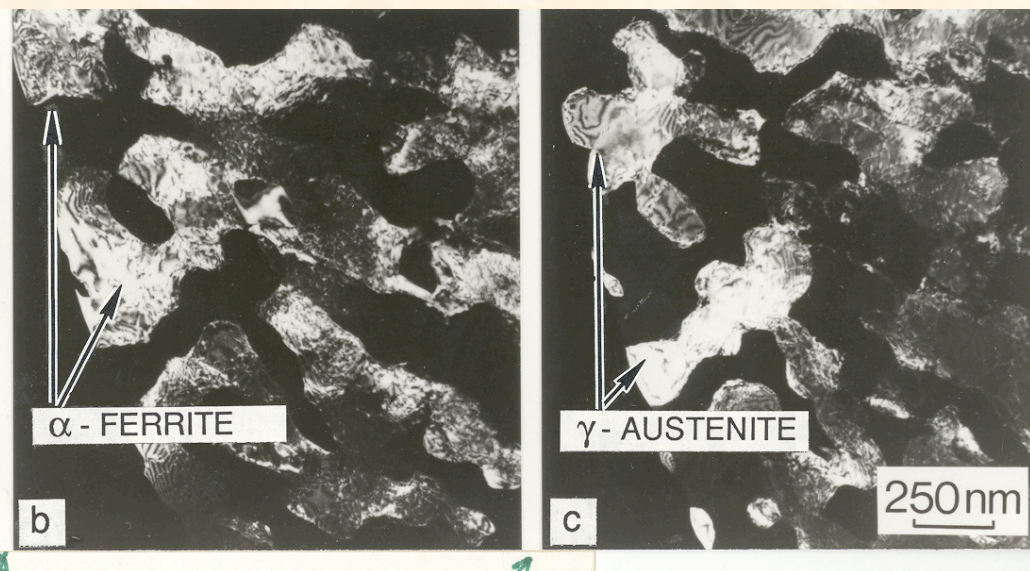


# Radiation-Induced Segregation Can Lead to Precipitation

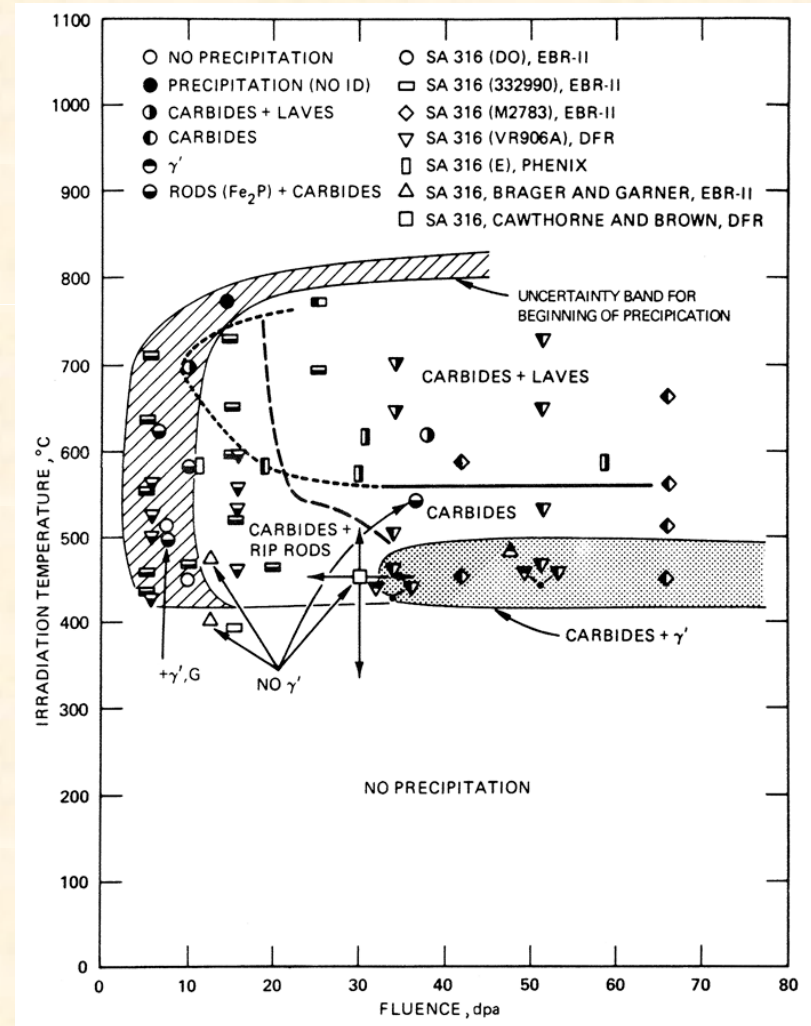
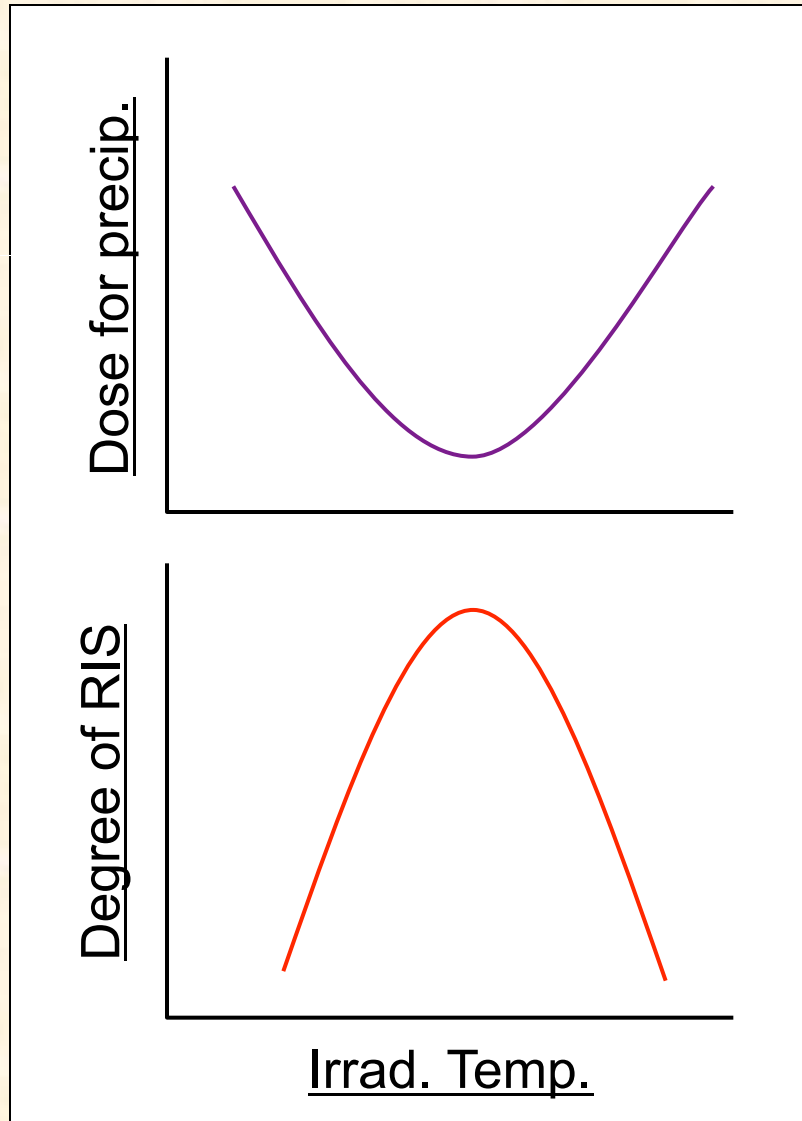


SA PCA steel irradiated at 500 C in ORR to 11 dpa (200 appm He), showing the association between radiation-induced G-phase silicide ( $\text{Mn}_6\text{Ni}_{16}\text{Si}_7$ ) particles and the largest voids

- Microstructure of SA Fe-12Cr-15Ni-1Si austenitic stainless alloy irradiated in EBR-II at 575°C (<20 dpa), with TEM showing
- RIS causes the initially homogeneous  $\gamma$ -austenite matrix to decompose into Fe-Cr-Si ferrite and Fe-Ni austenite.



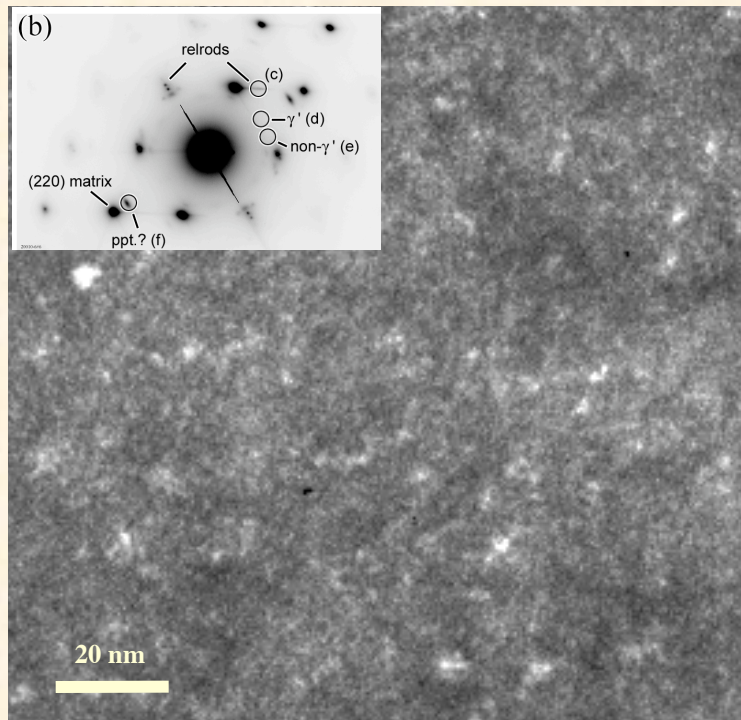
# RIS and RIP will be very sensitive to the operating conditions



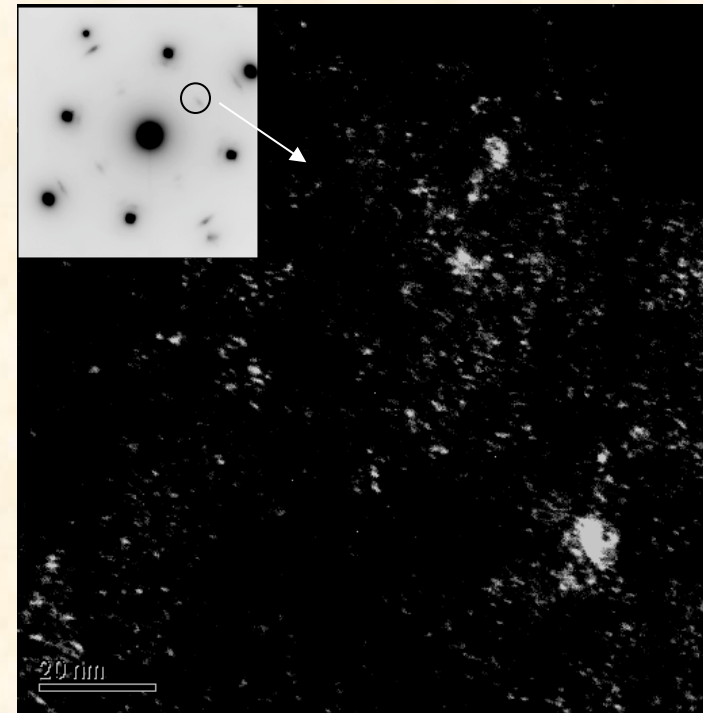
RIS and RIP have been widely observed in 316 SS alloys, and occurs in many other alloy systems.



# Comparison of $\gamma'$ in proton- and neutron-irradiated SS



**Tihange baffle bolt:**  
neutron-irradiated to ~7 dpa  
at 299°C\*.



**304+Si** proton-irradiated to  
5.5 dpa at 360°C.

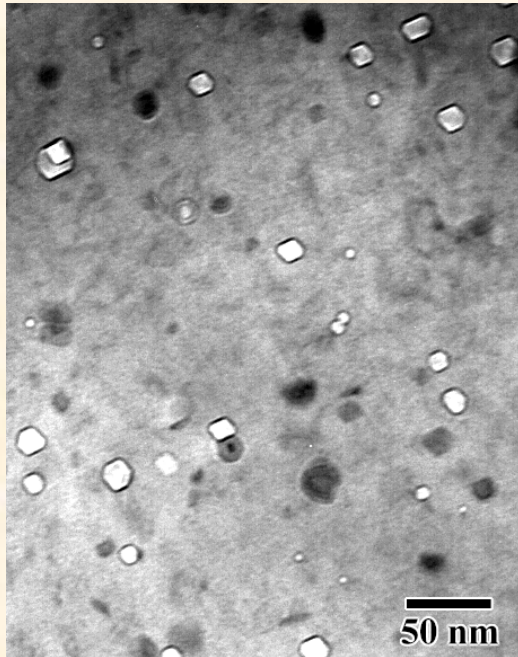
- *ATEM Characterization of Stress-Corrosion Cracks in LWR-Irradiated Austenitic Stainless Steel Core Components, PNNL EPRI Report, 11/2001.*
- *Image resized for equivalent scale.*

# **Fundamentals of Radiation Damage**

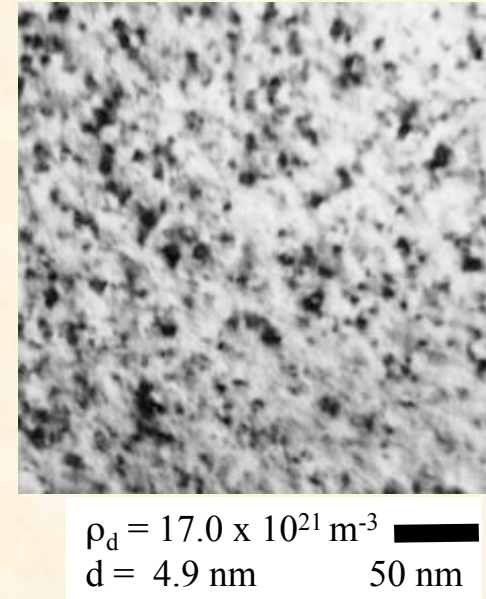
## **Clustering-related forms of radiation-induced degradation**



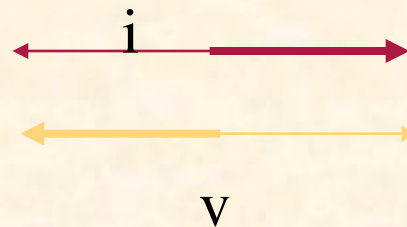
# Clusters: voids and dislocation loops



- Process
  - Radiation produces point defects
  - Interstitials migrate preferentially to dislocations leaving excess vacancies to form voids
  - Both grow as they absorb more defects

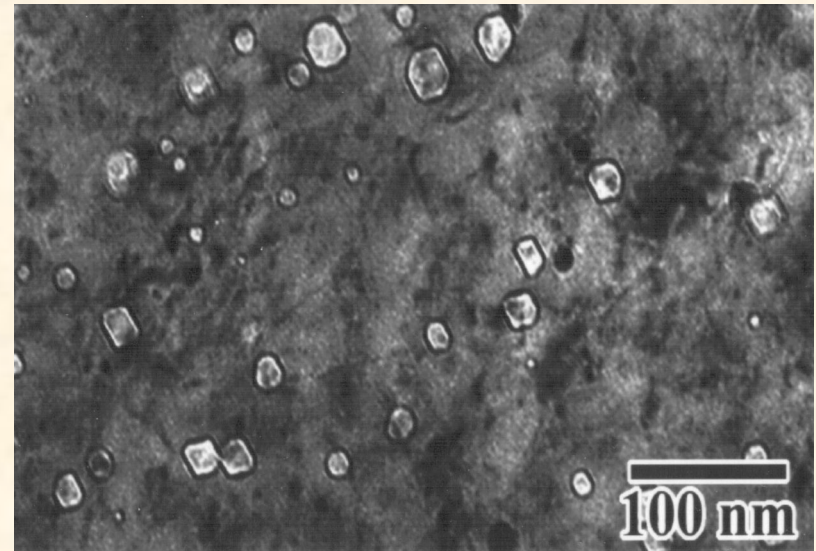
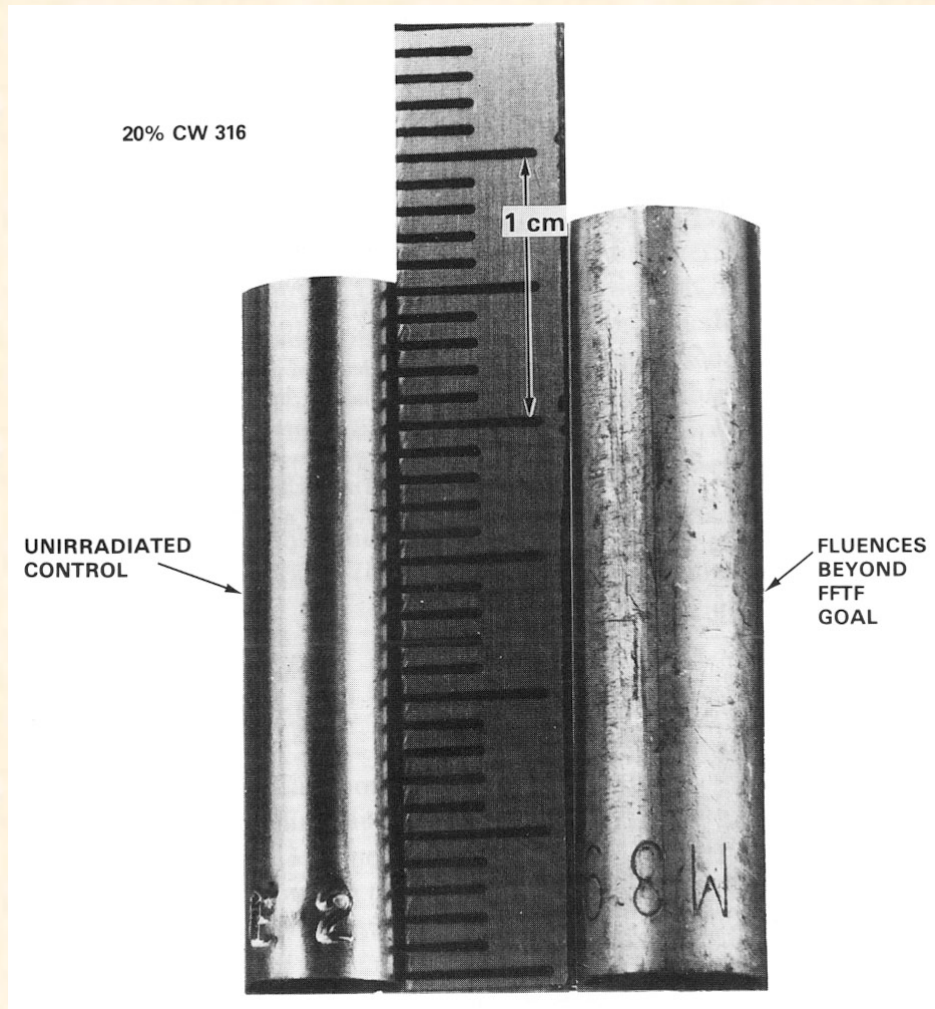


Void

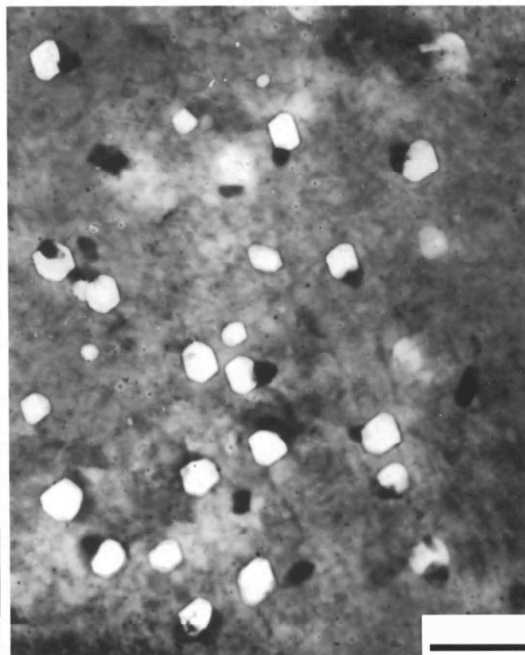
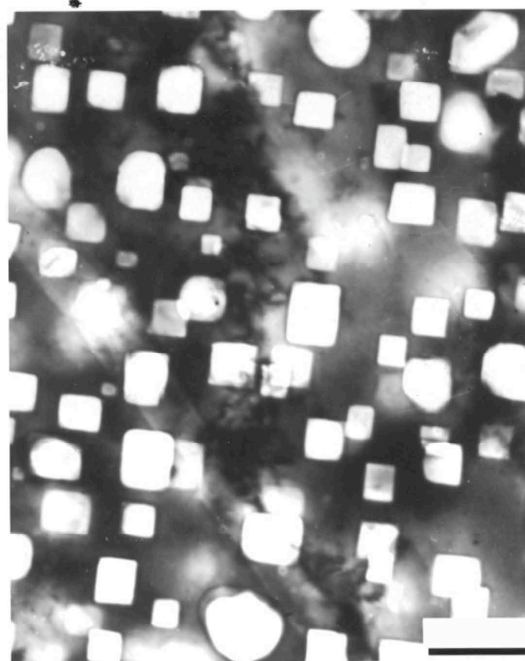
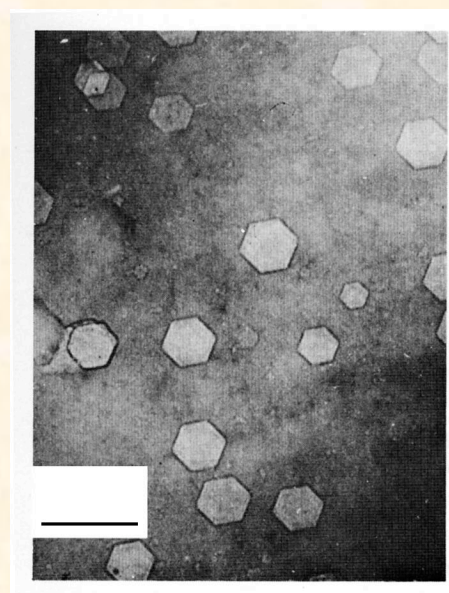
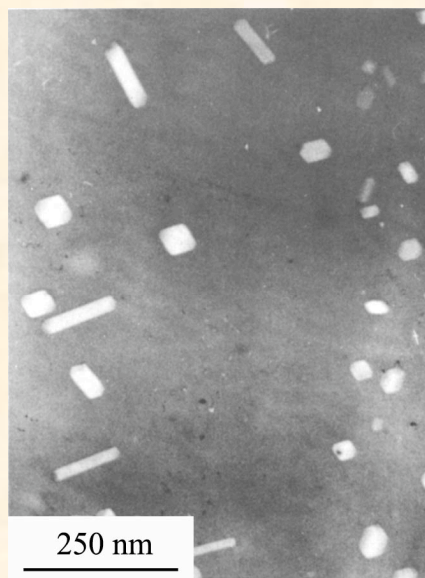


Dislocation loop

# Swelling is readily observed in many steels under various reactor conditions



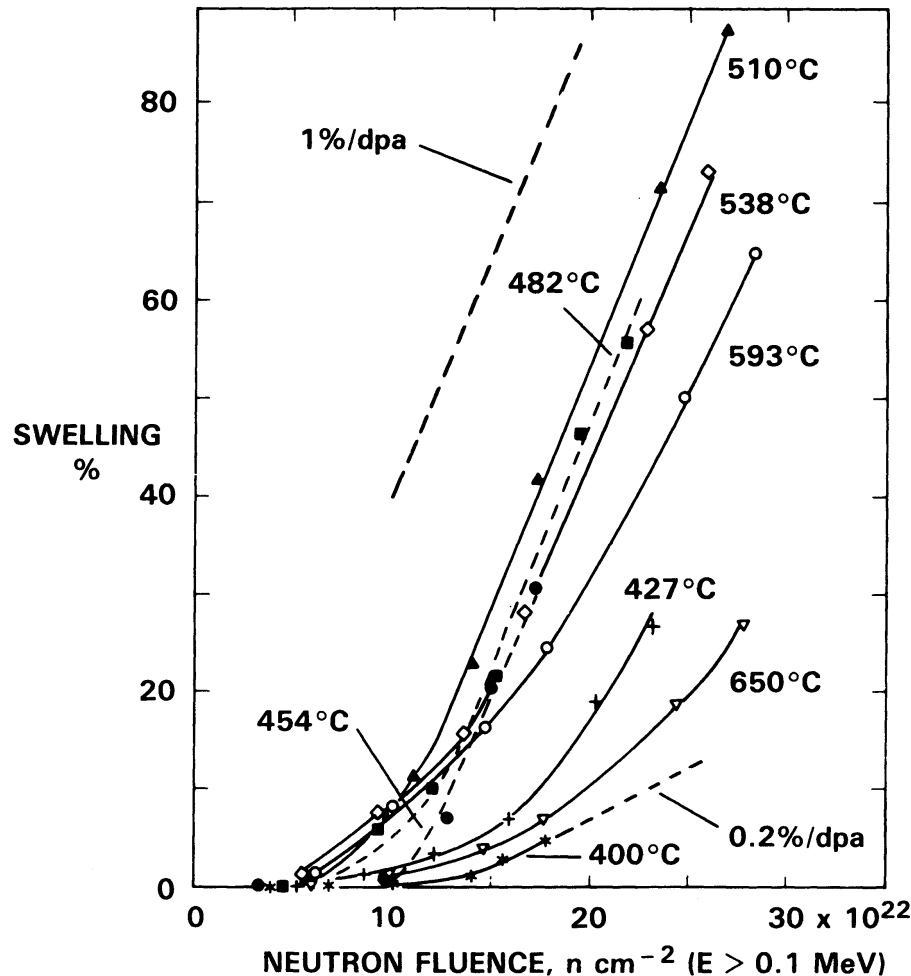
Source: F. Garner





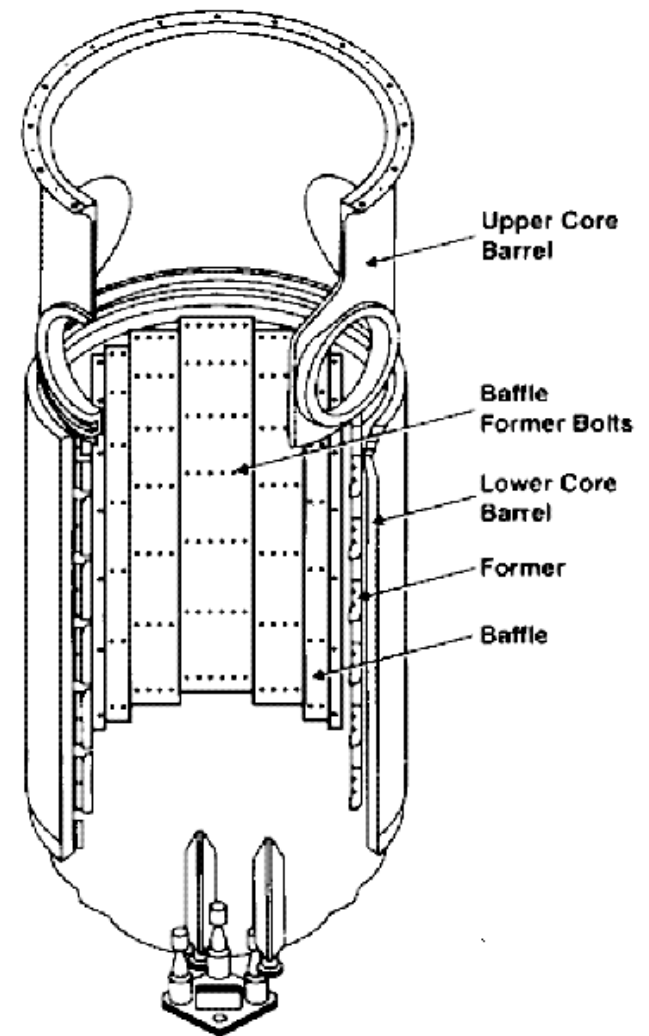
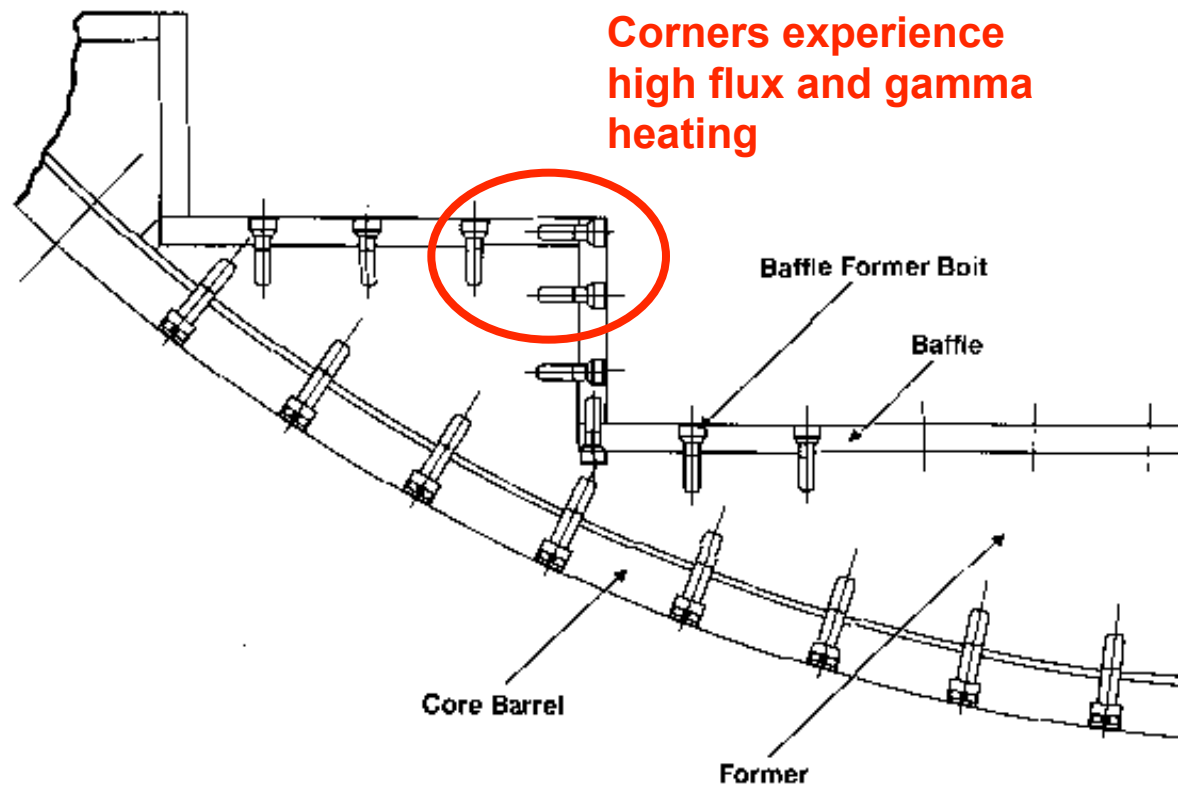
# Swelling of 20% CW 316 stainless steel in EBR-II

(Garner and Gelles, 1990)

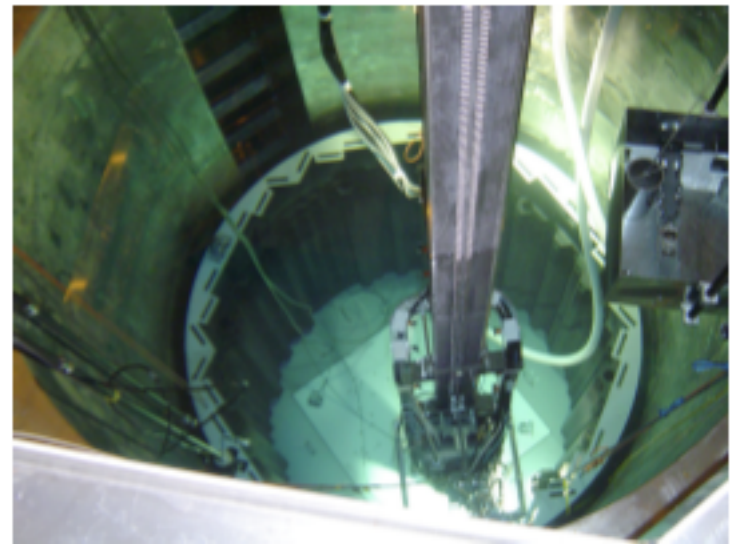
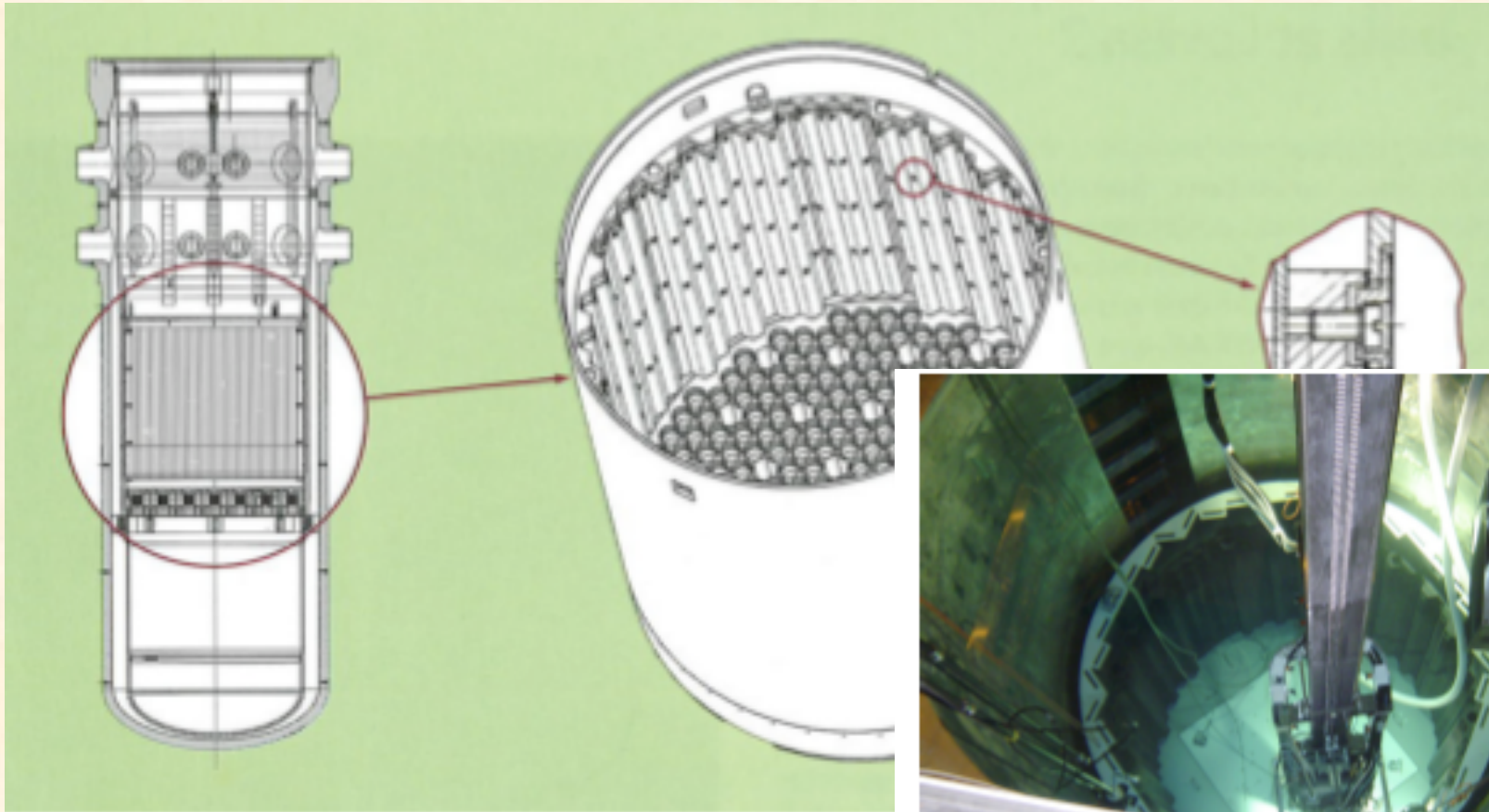


- ▶ Swelling occurs above temperatures above  $\sim 300^\circ\text{C}$ .
- ▶ The eventual swelling rate of 316 at all temperatures is  $\sim 1\%/dpa$ .
- ▶ The temperature dependence lies only in the duration of the transient regime.
- ▶ The transient regime is very sensitive to any material or environmental variable.

# Baffle bolts experience some of the highest fluences and temperatures in a PWR core



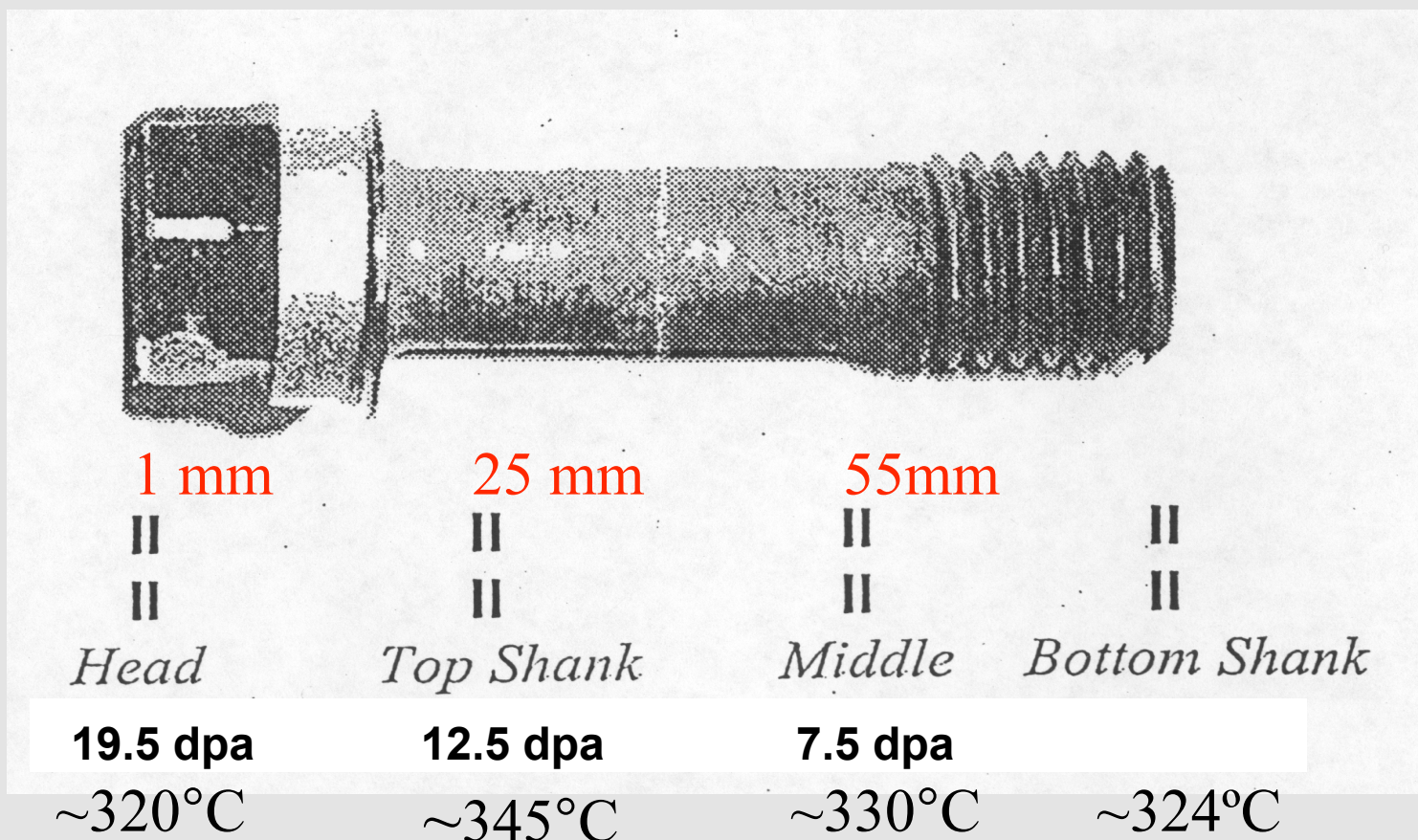
# Baffle bolts experience some of the highest fluences and temperatures in a PWR core





# Cutting diagram for 15% cold-worked 316 baffle bolt after 20 years in a PWR

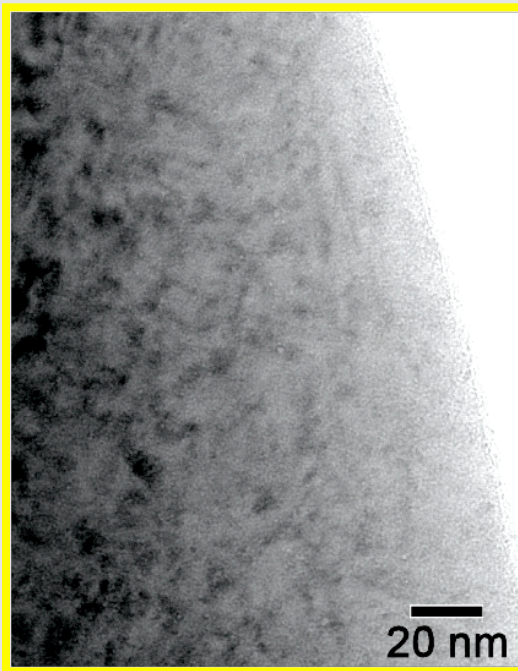
Edwards, Garner, Oliver and Bruemmer, 2003



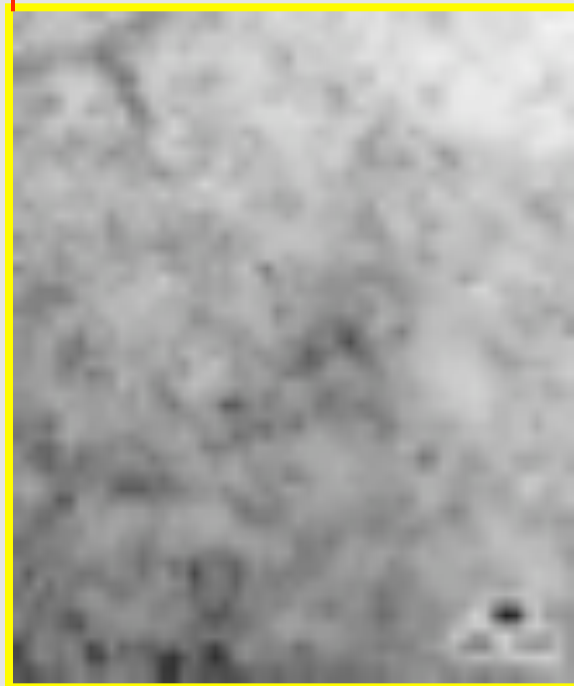
# Swelling and **helium** content observed in CW 316SS baffle-former bolt

Edwards, Garner, Oliver and Bruemmer, 2003

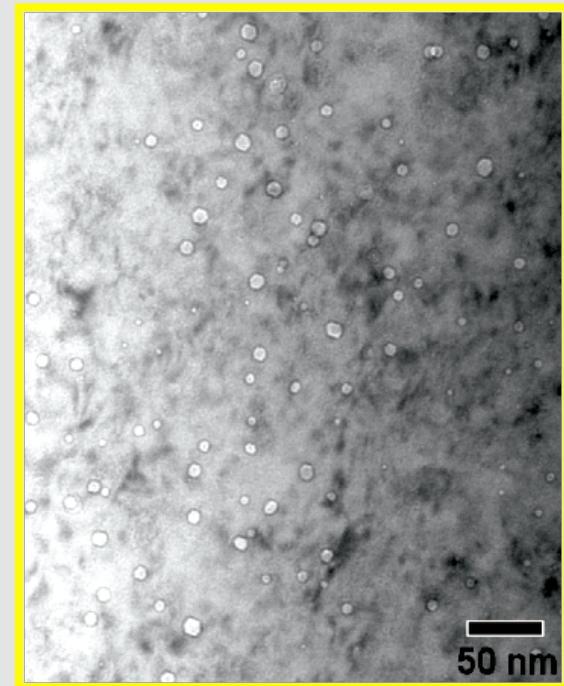
<.0.01%, 71 appm Helium; Both at ~0.2% swelling , 53 and 49 appm Helium



Bolt Head, 1 mm  
19.5 dpa, ~320°C



Top Shank, 25 mm  
12.5 dpa, ~343°C

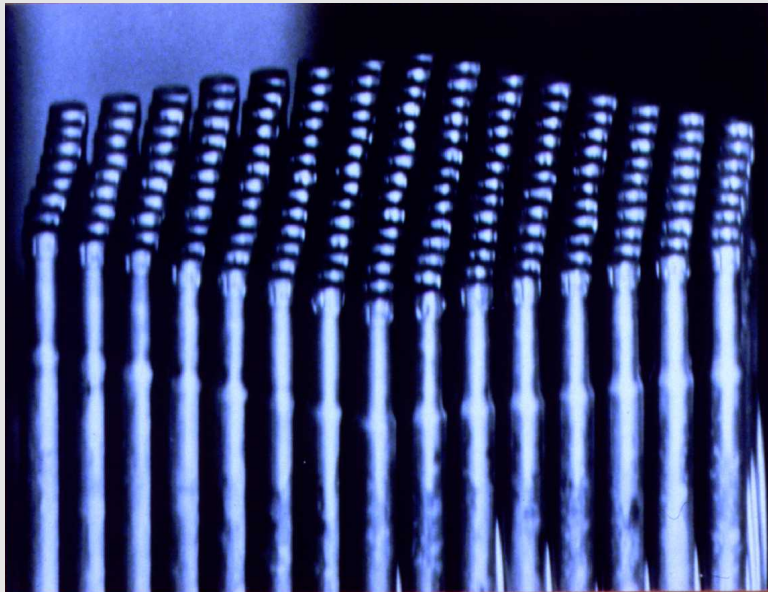


Near Threads, 55 mm  
7.5 dpa, ~333°C

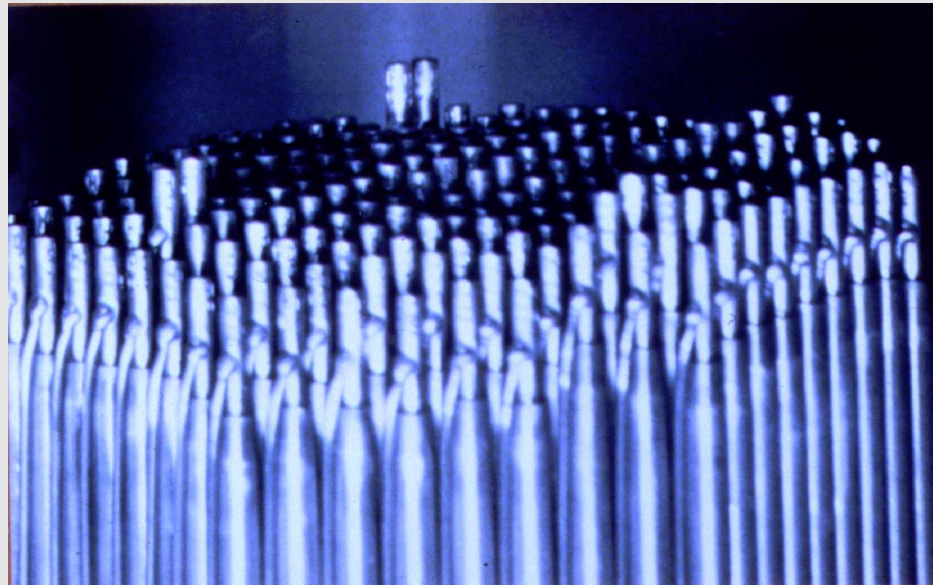


# Swelling can create tolerance problems

## FFTF Fuel Pin Bundles

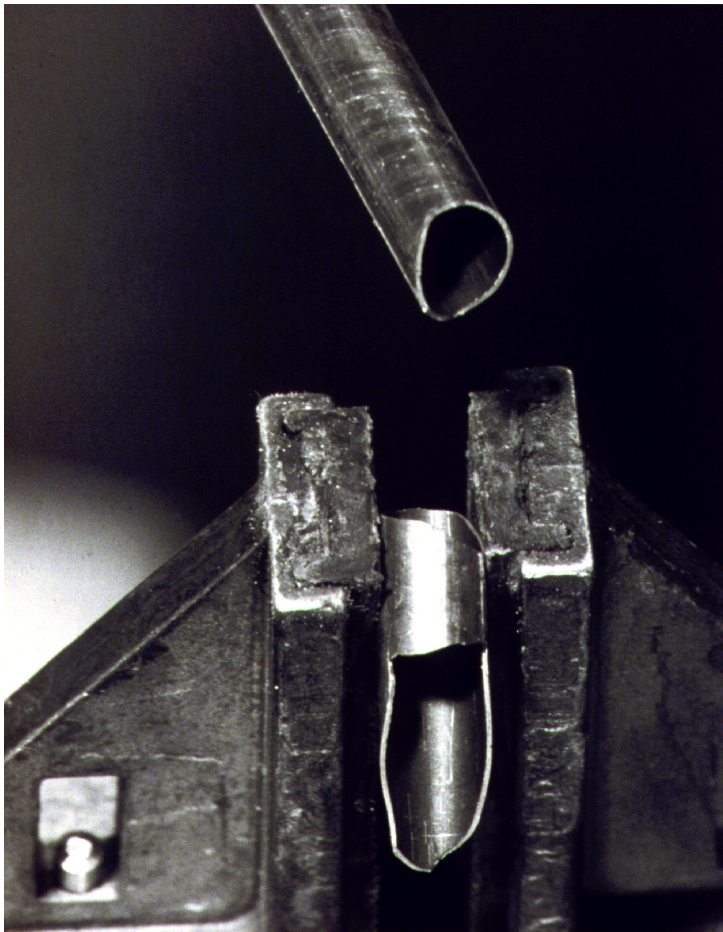


HT-9, no swelling



316-Ti stainless, swelling

# Severe void-induced embrittlement

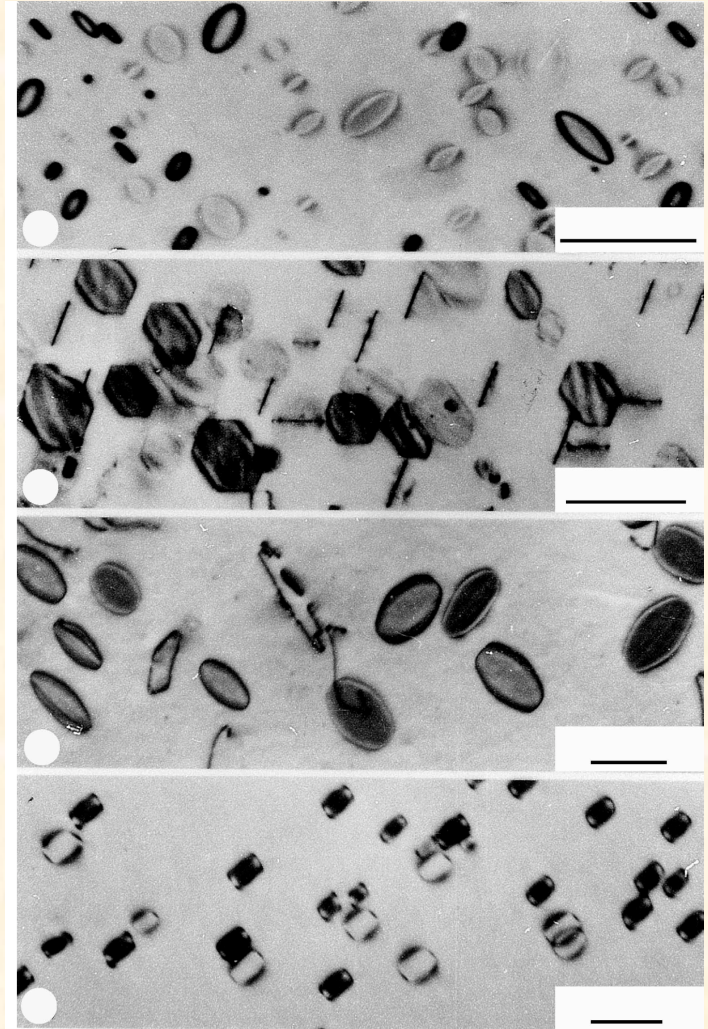
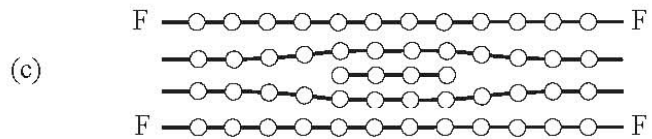
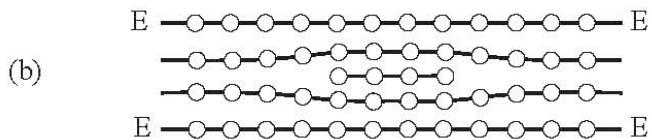
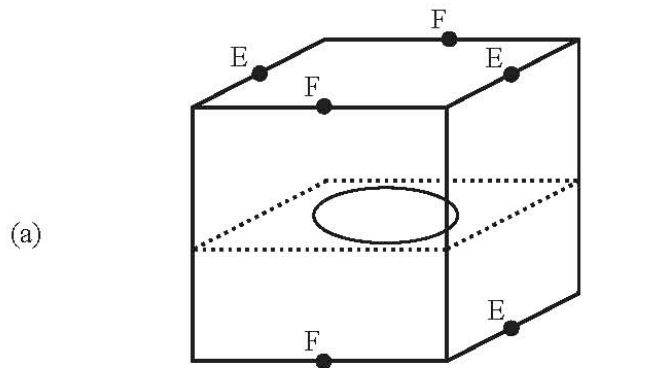


- 14% swelling
- Failure occurred during clamping in a vise at room temperature.
- Tearing modulus has fallen to zero, with no resistance to crack propagation.
- 316 stainless steel irradiated at  $\sim 400^{\circ}\text{C}$
- **Embrittlement threshold at  $\geq 10\%$  swelling.**

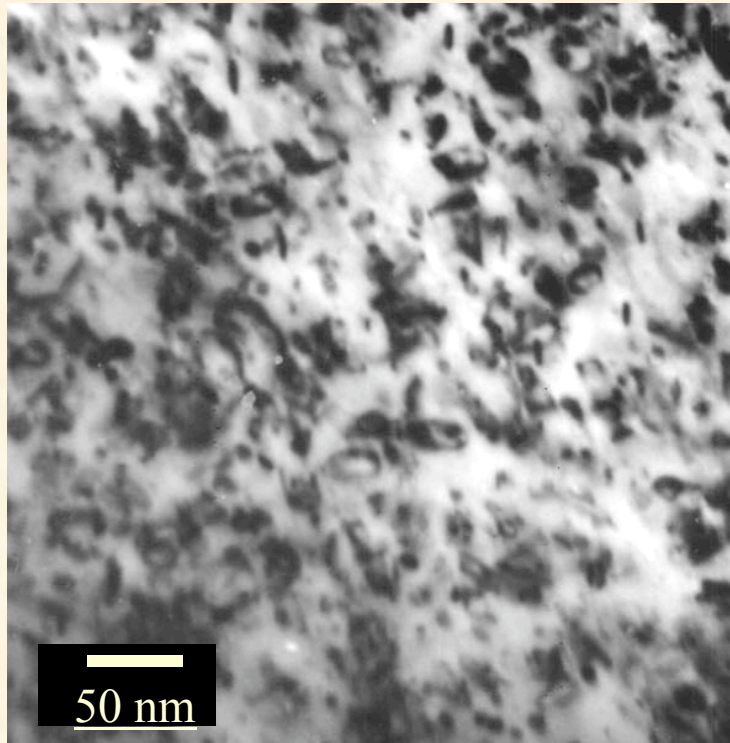


# Interstitials (or vacancies) can also cluster into discs

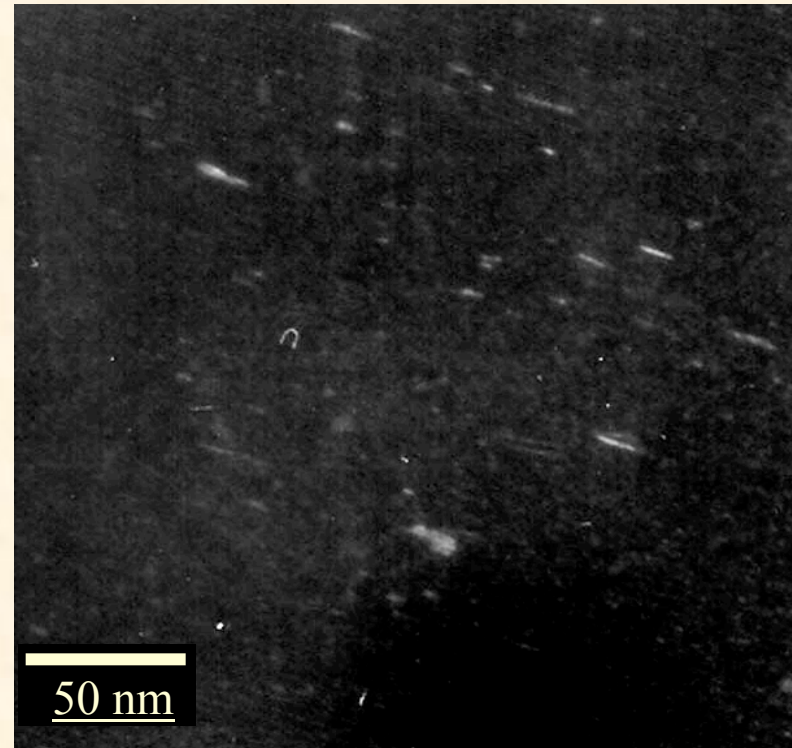
## Faulted (Frank) Loop



# Dislocation loop microstructure is observed using transmission electron microscopy



Bright Field

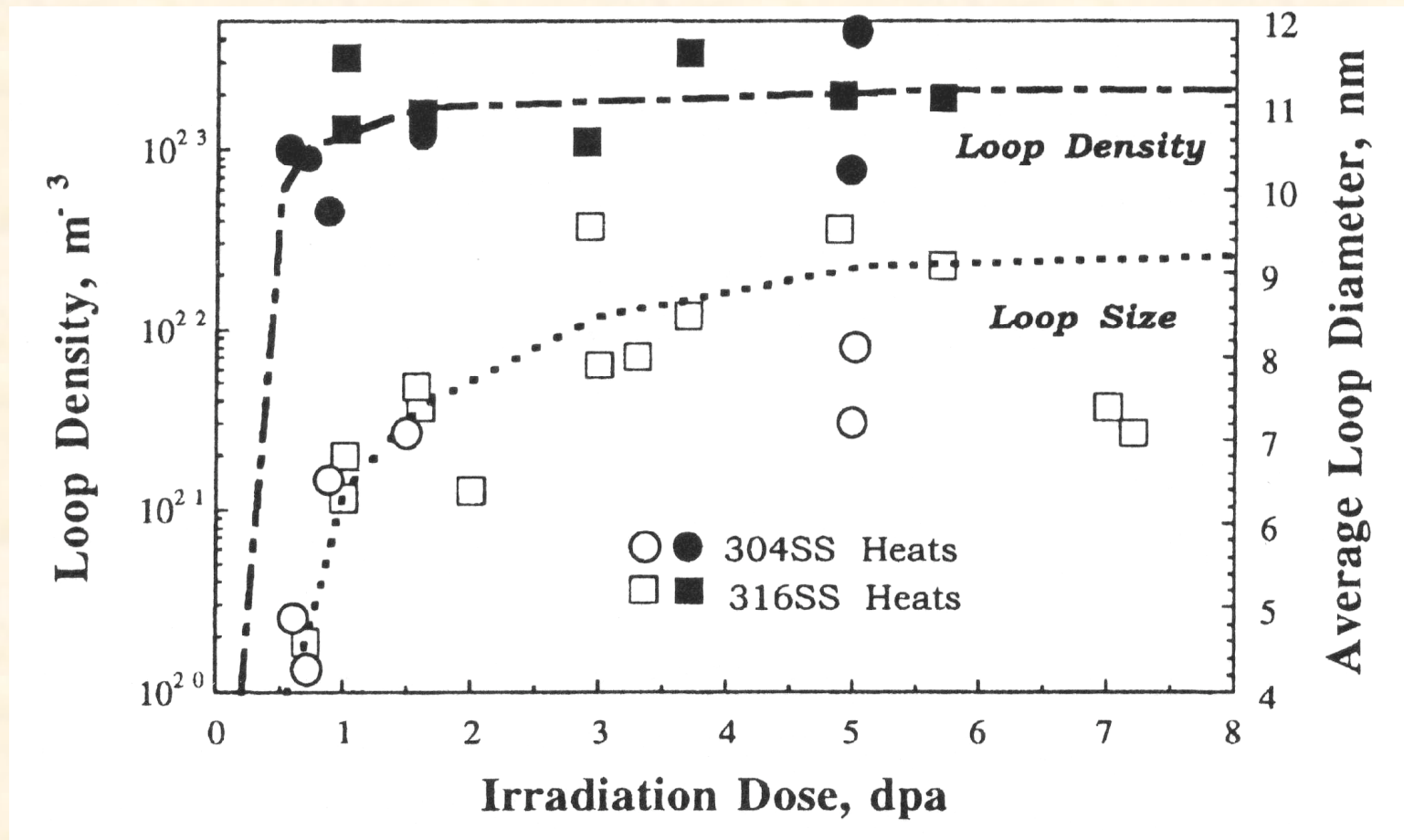


Dark Field

CP-304 SS irradiated to 0.55 dpa with protons at 360°C



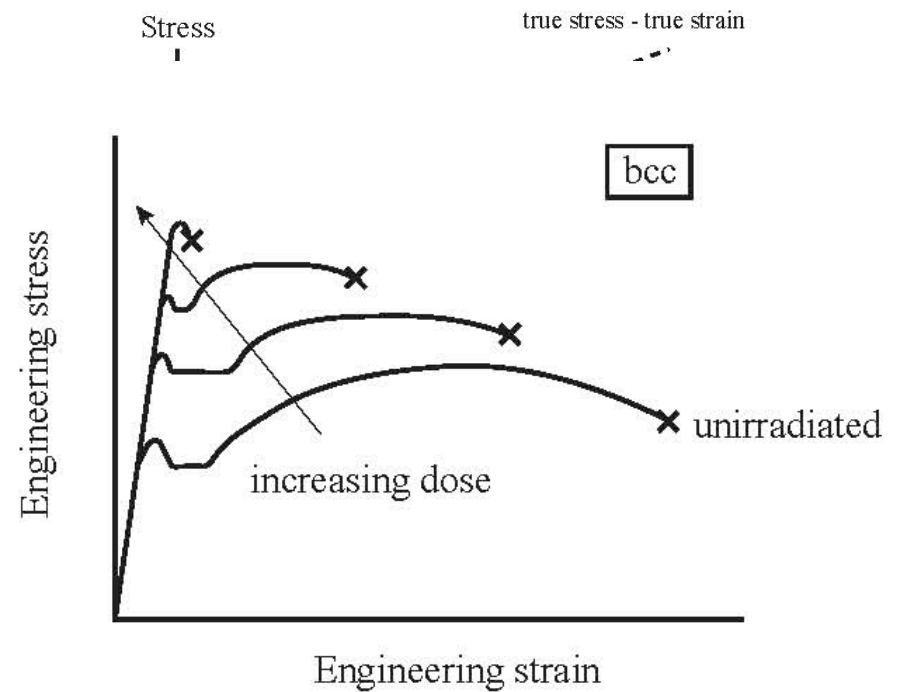
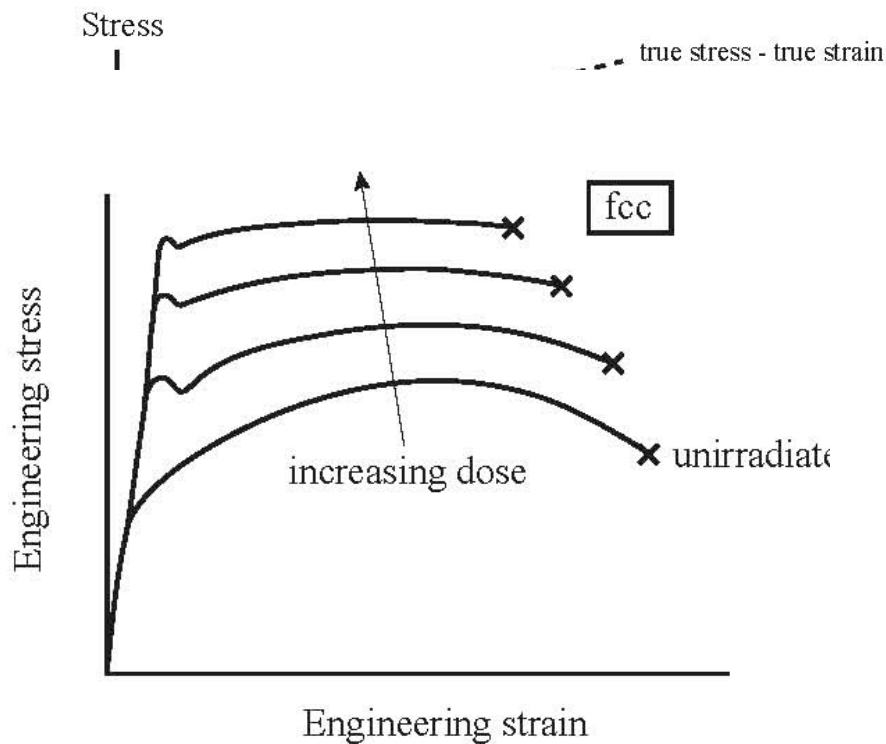
# Behavior of Dislocation Loop Size and Number Density



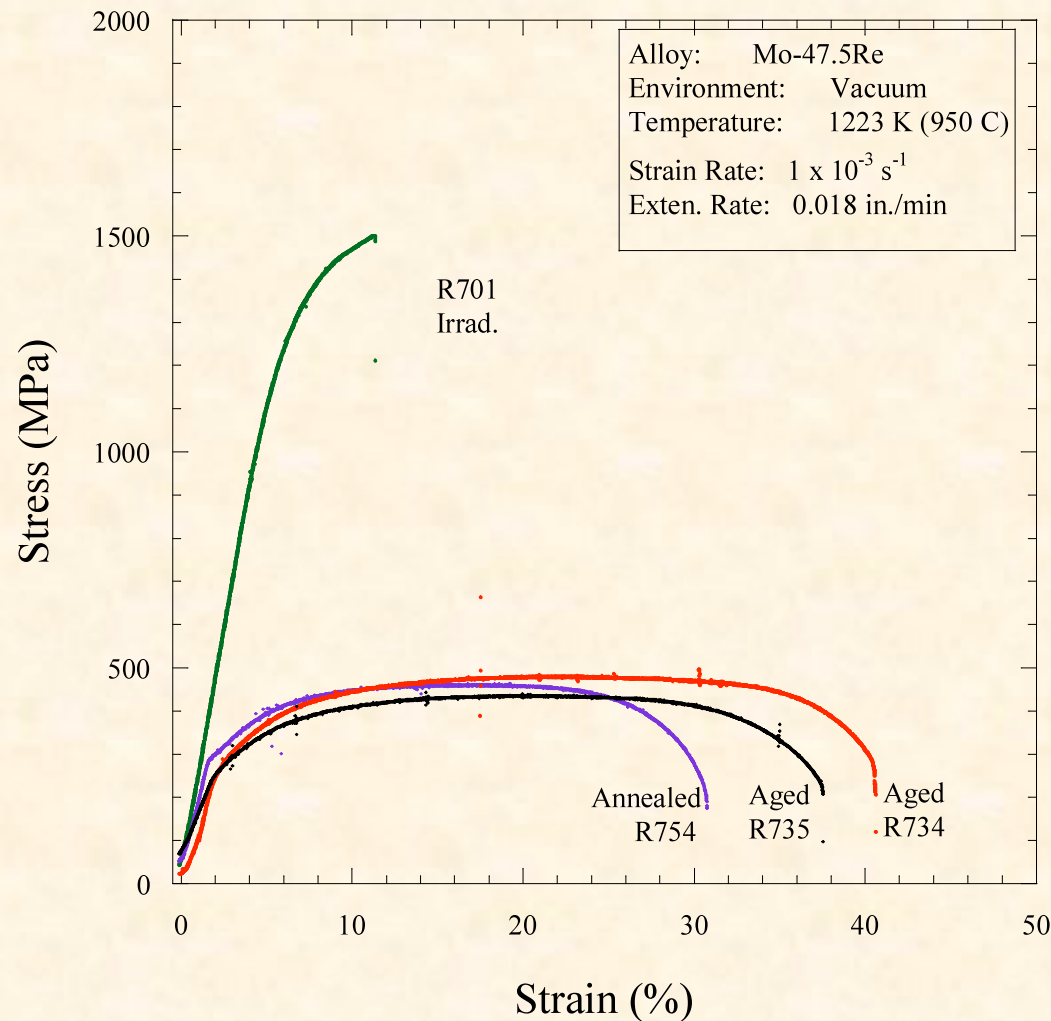
# Irradiation-induced defects and microstructure also influence stress-strain curves

fcc

bcc

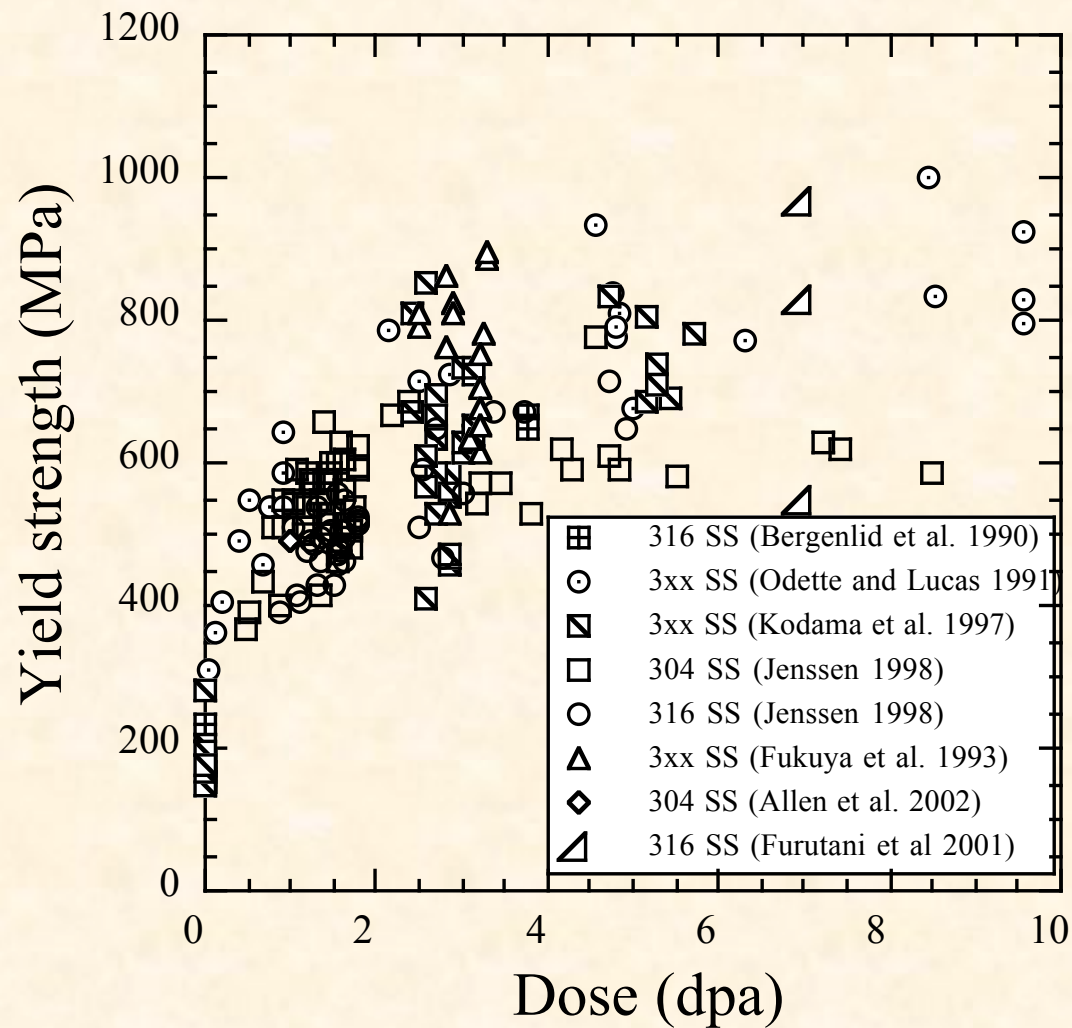


# Radiation hardening is observed in many classes of materials

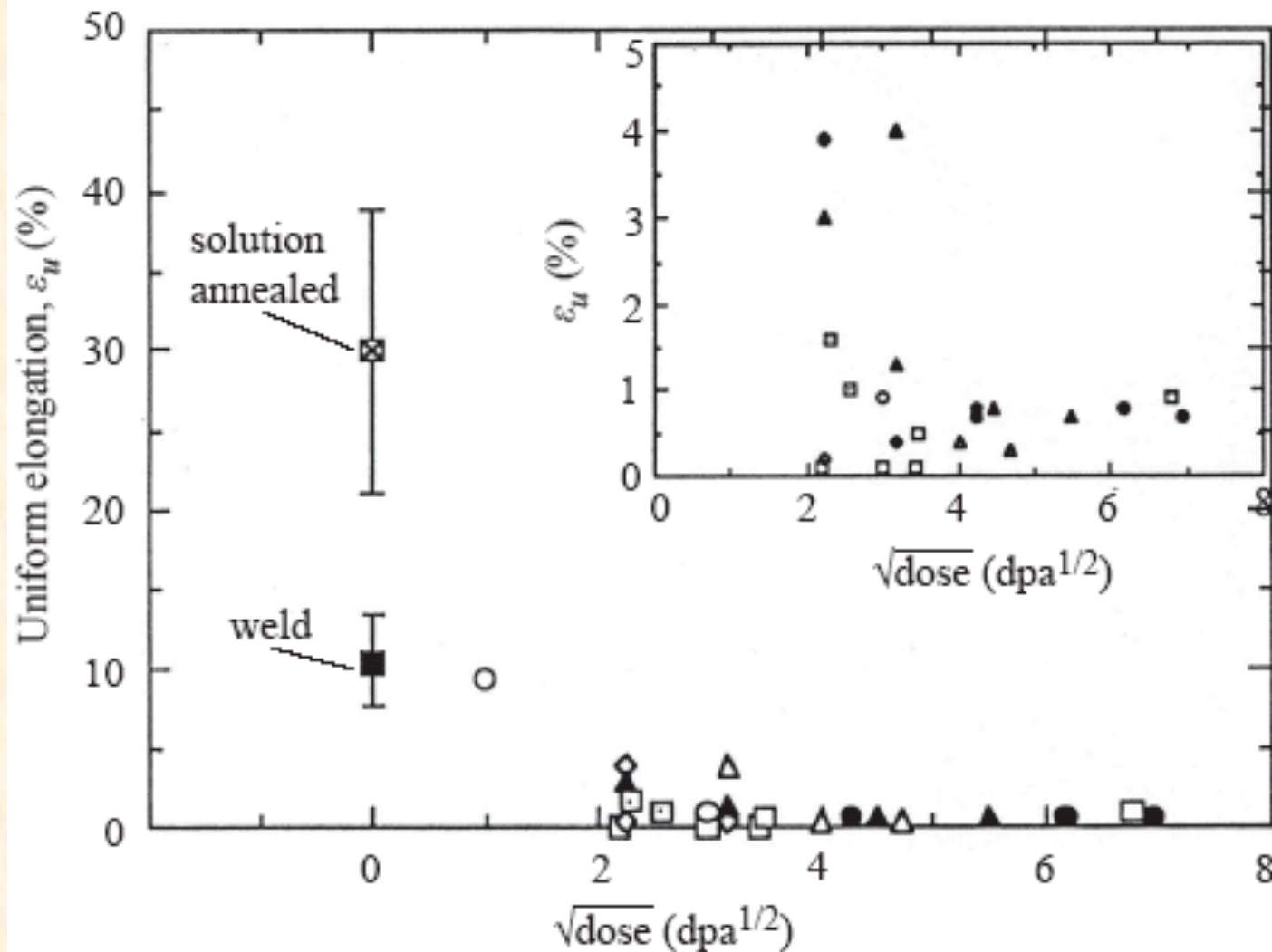


- This hardening is also observed in many different materials.
- Increases in YS and UTS are commonly observed.
- Irradiation also results in a drop in ductility.

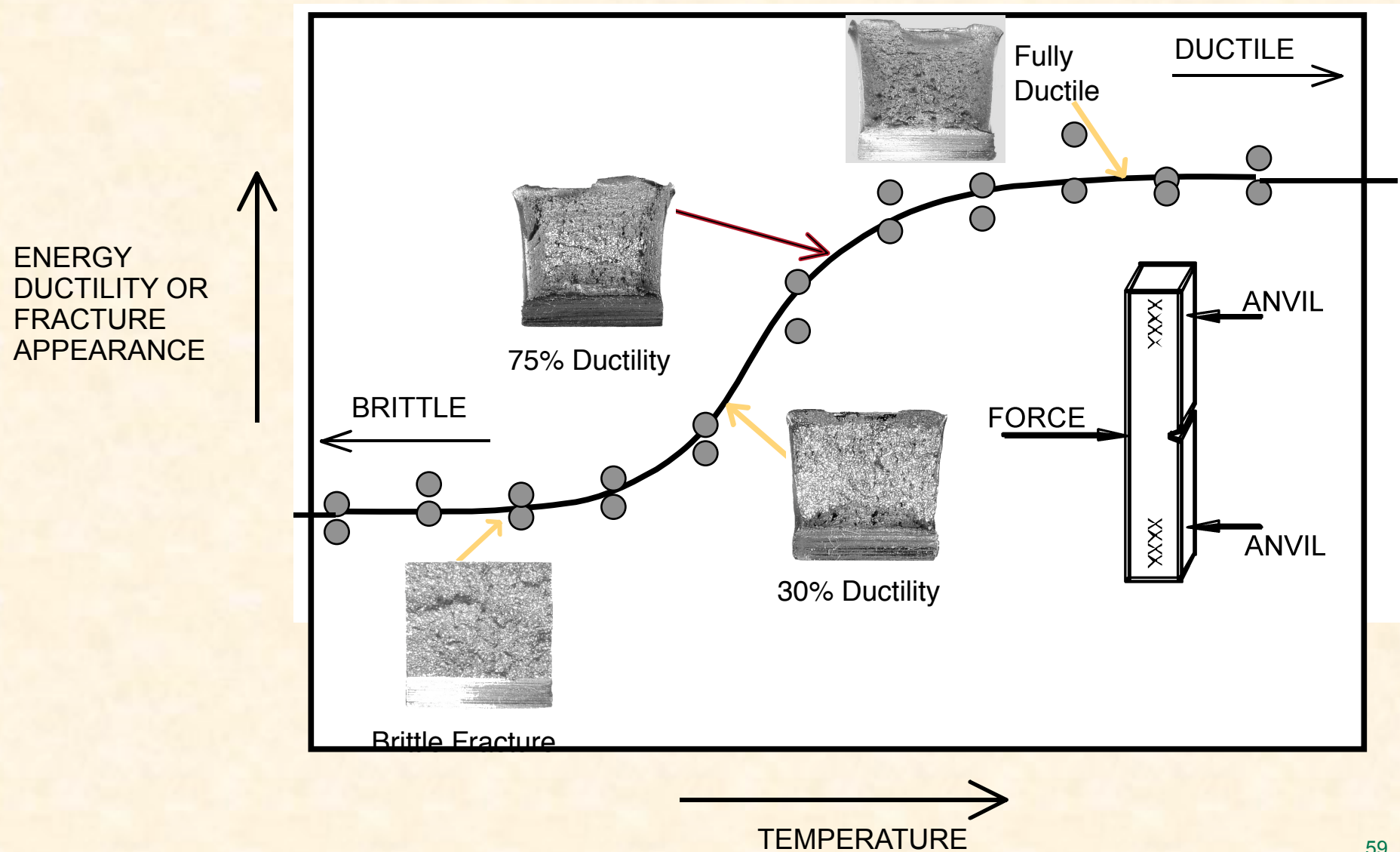
# Irradiation hardening is widely studied in stainless steels



# Hardening also results in a loss of ductility

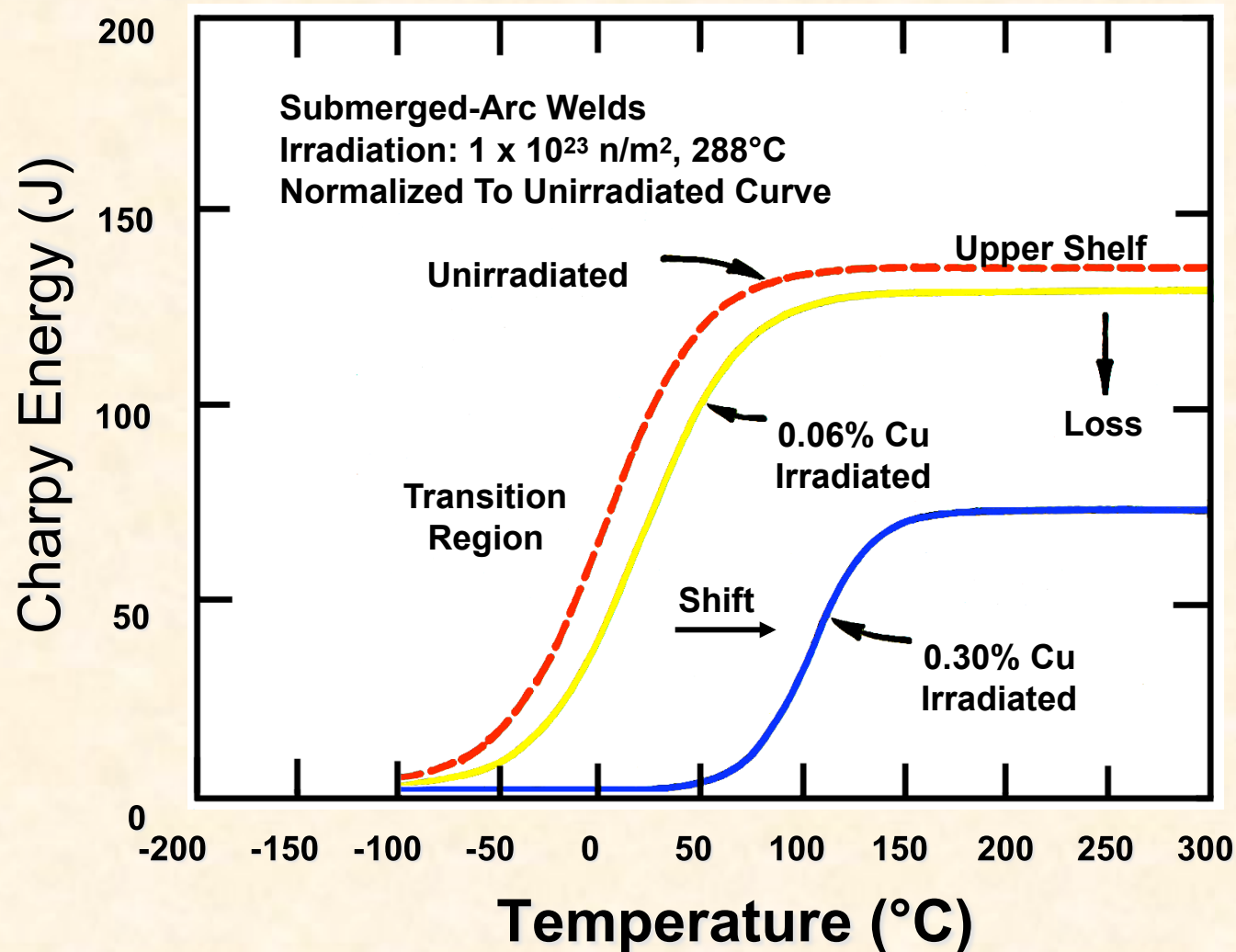


# Loss of ductility can lead to loss of toughness or even brittle failure



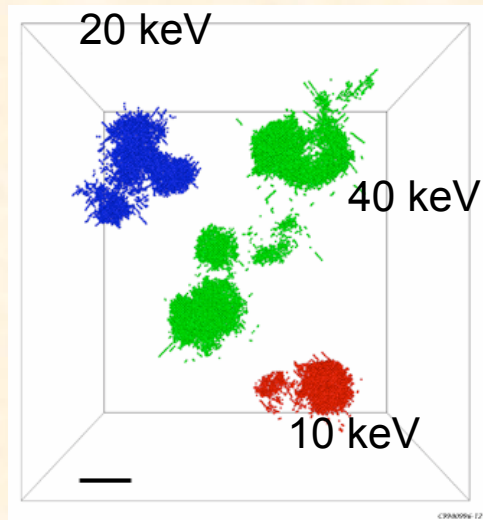


# Radiation-embrittlement and the DBTT are a key concern in RPV steels

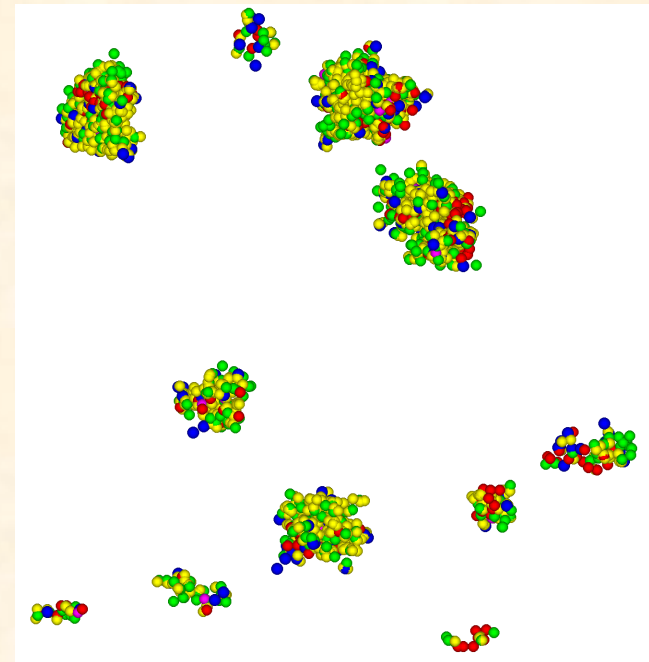
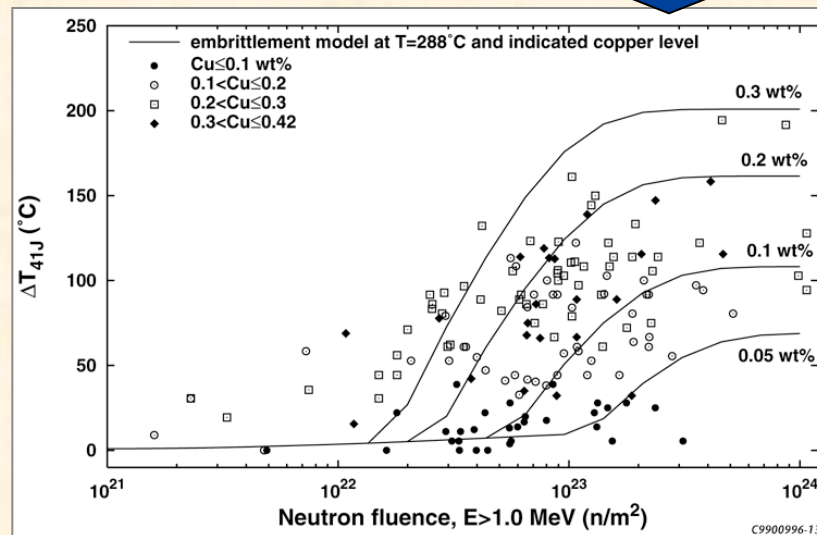


**Irradiation Causes Ductile/Brittle Transition Temperature Shift and Upper Shelf Energy Loss — Copper Increases The Effect**

# Microstructural Investigations Such As Atom Probe Tomography Are Used to Reveal Mechanisms of Irradiation Embrittlement



Neutron radiation produces an extremely high number density of nanoscale copper-, manganese-, nickel-, silicon-, and phosphorus-enriched precipitates.



Fe Cu Ni Mn Si P atoms

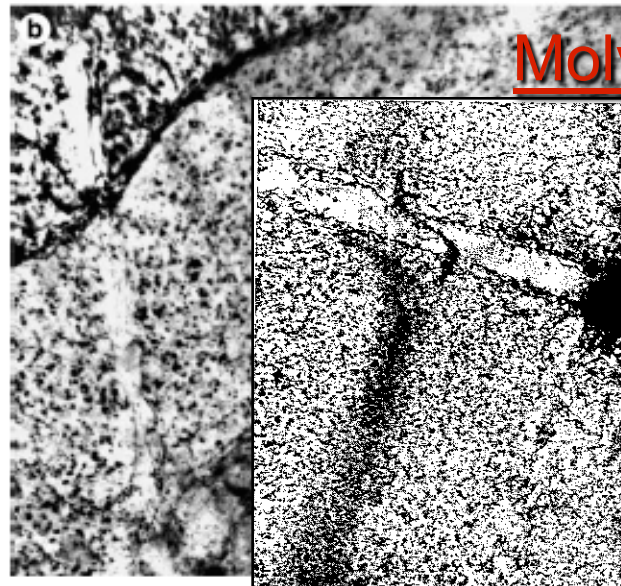
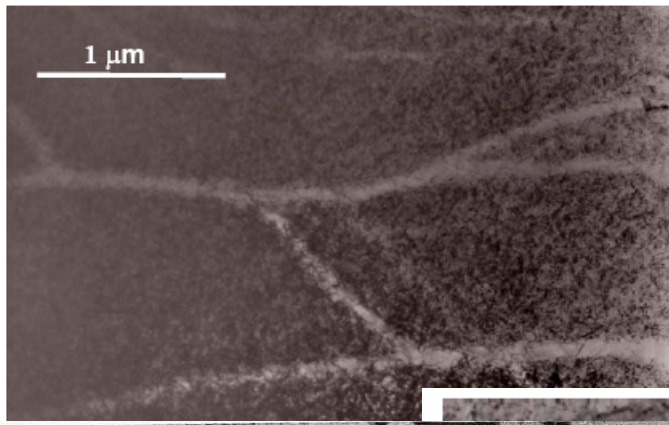
Combination of experimental, modeling, and microstructural studies leads to advances in predictive capability.

# **Fundamentals of Radiation Damage**

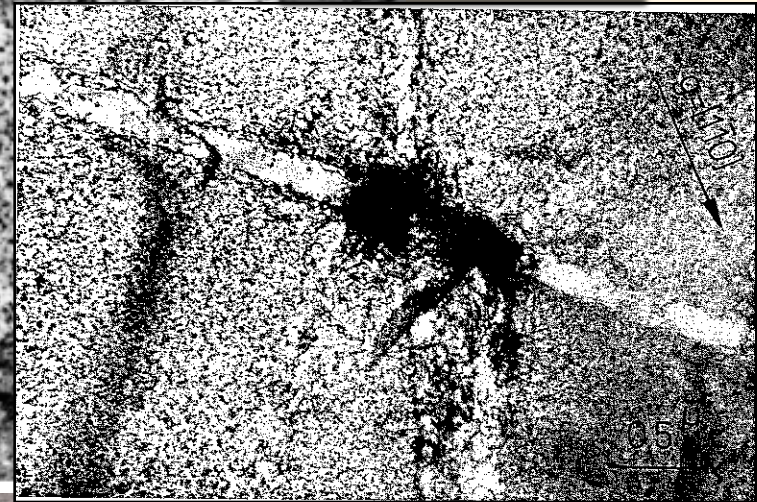
**Other forms of degradation that don't fit above, but are still really important!**



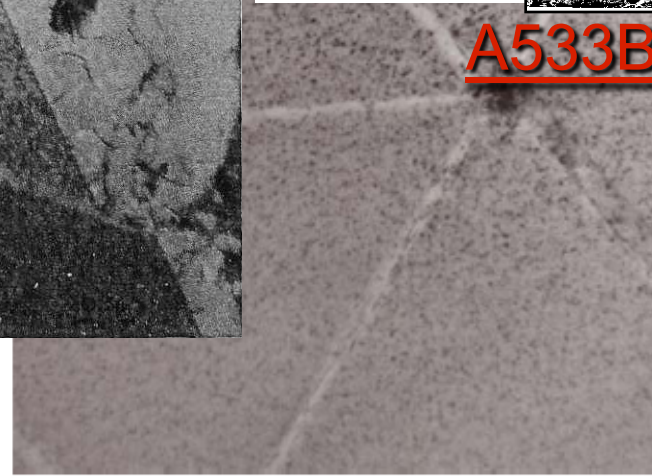
# Localized Deformation Occurs In Many Irradiated Material Systems



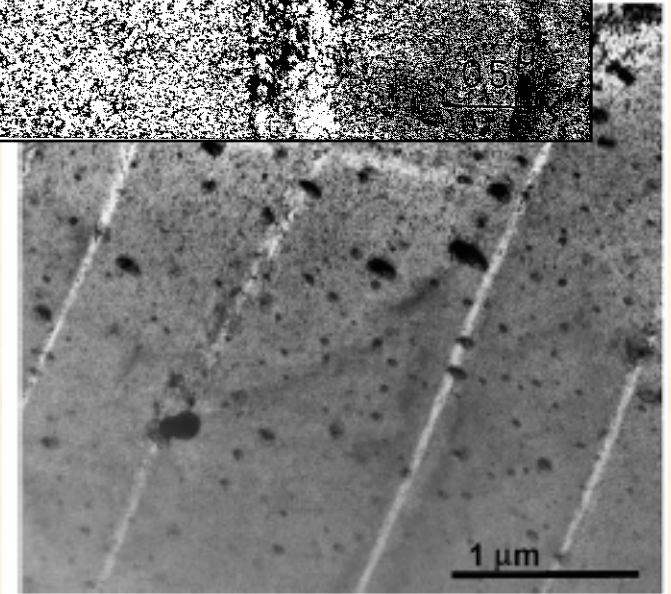
Molybdenum



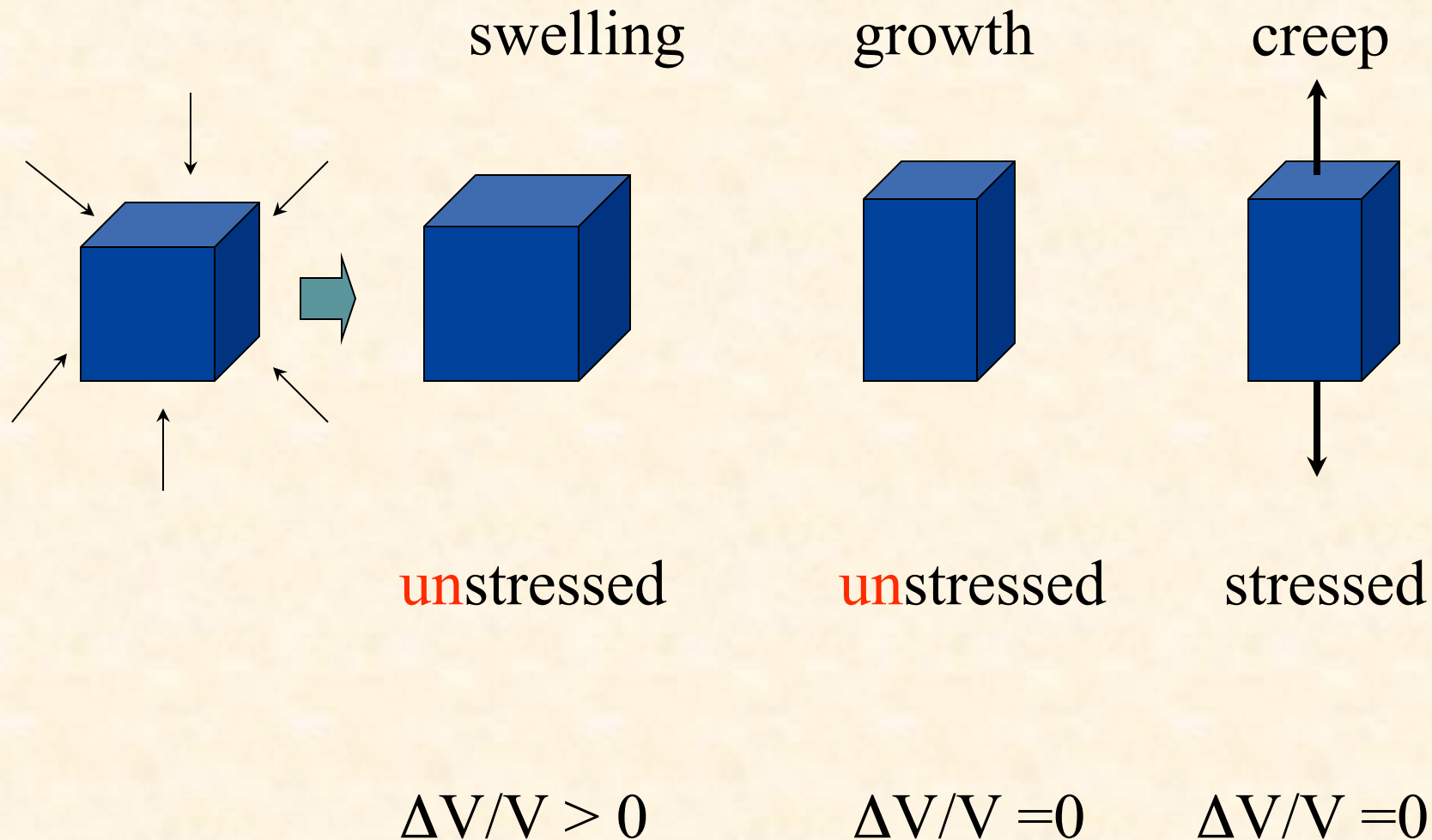
Copper



316 SS

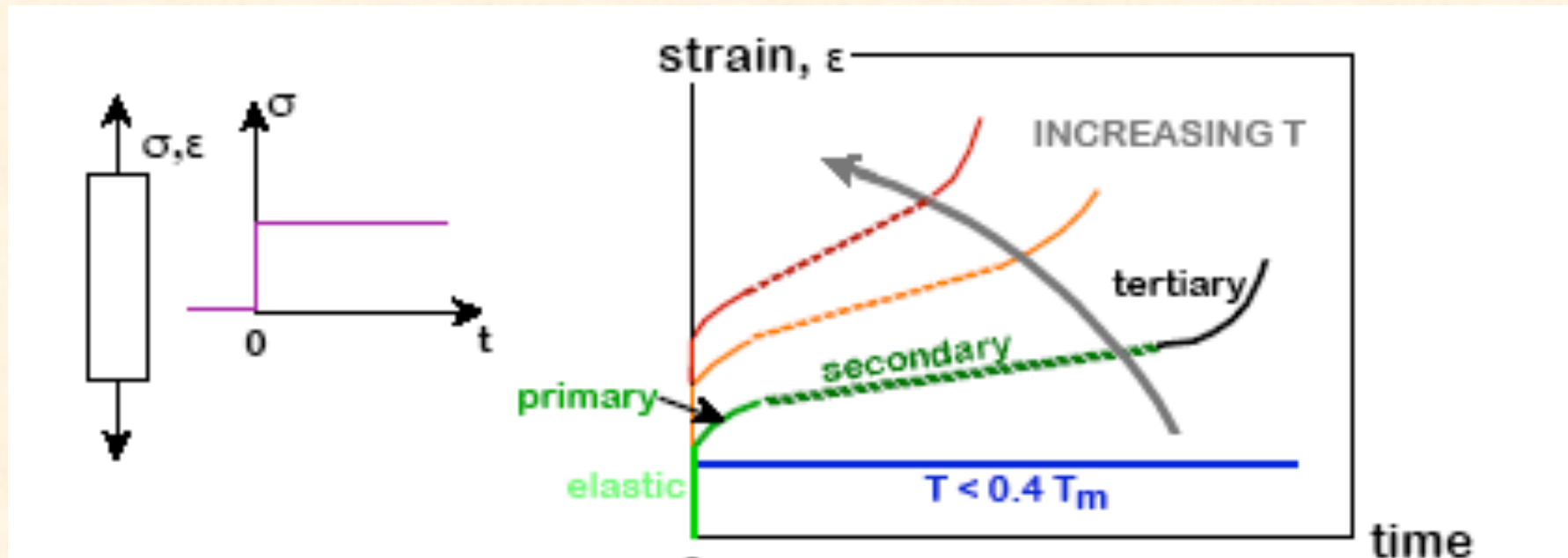


# Dimensional stability is heavily influenced by irradiation



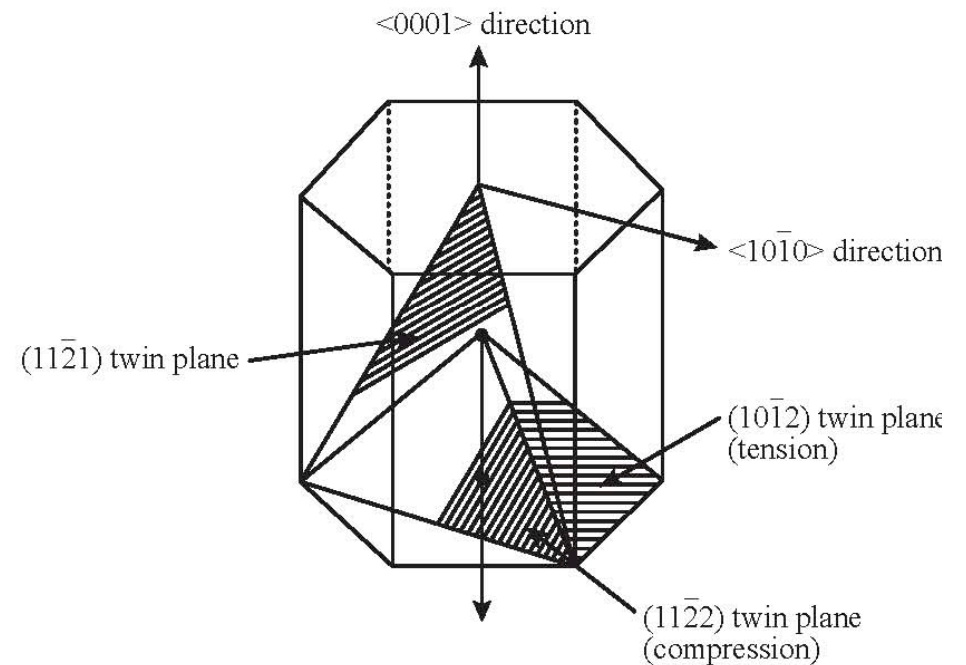
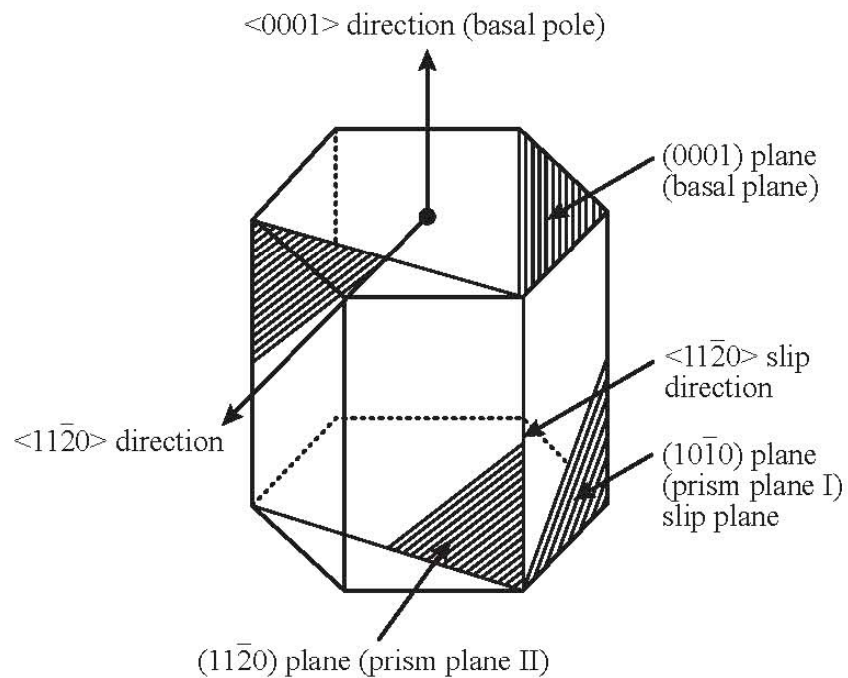


# Irradiation also influences creep processes

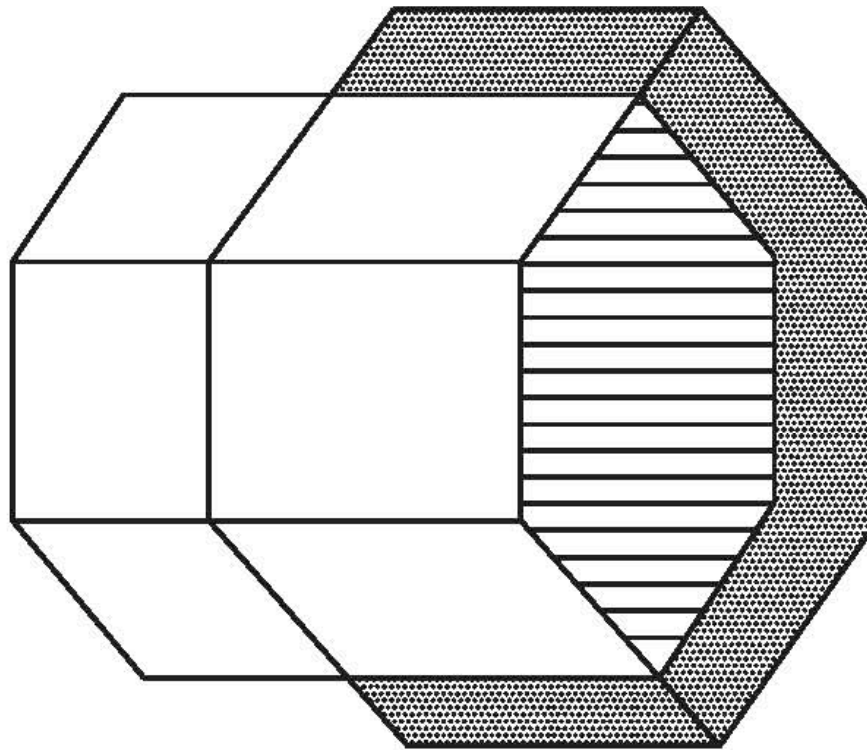


- Radiation produced point defects increase diffusion and allow creep at lower temperatures

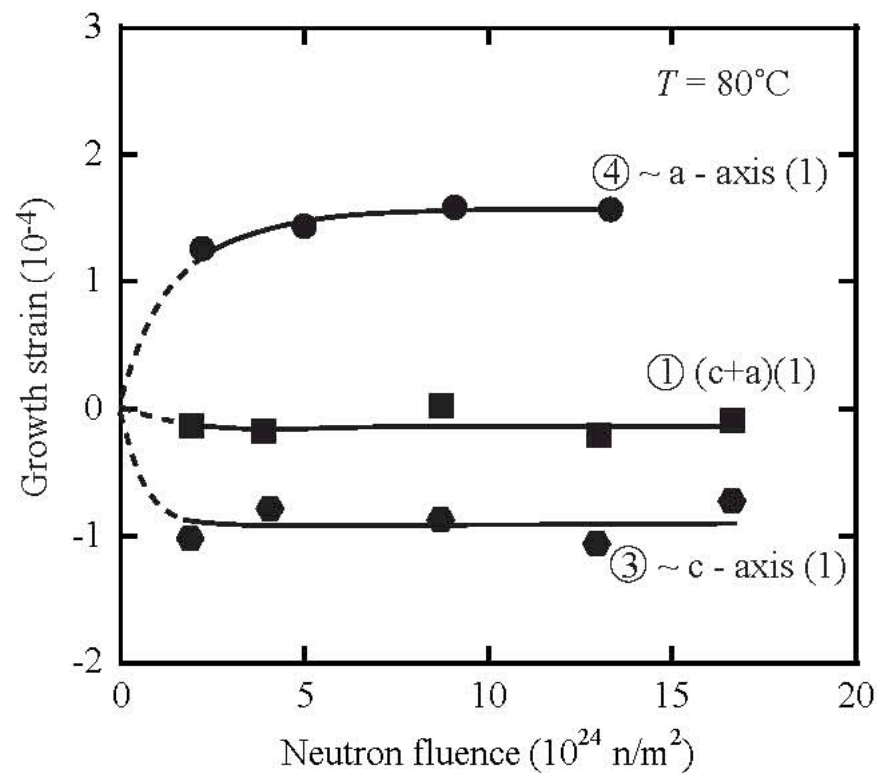
# Growth is a common issue in Zr-alloys



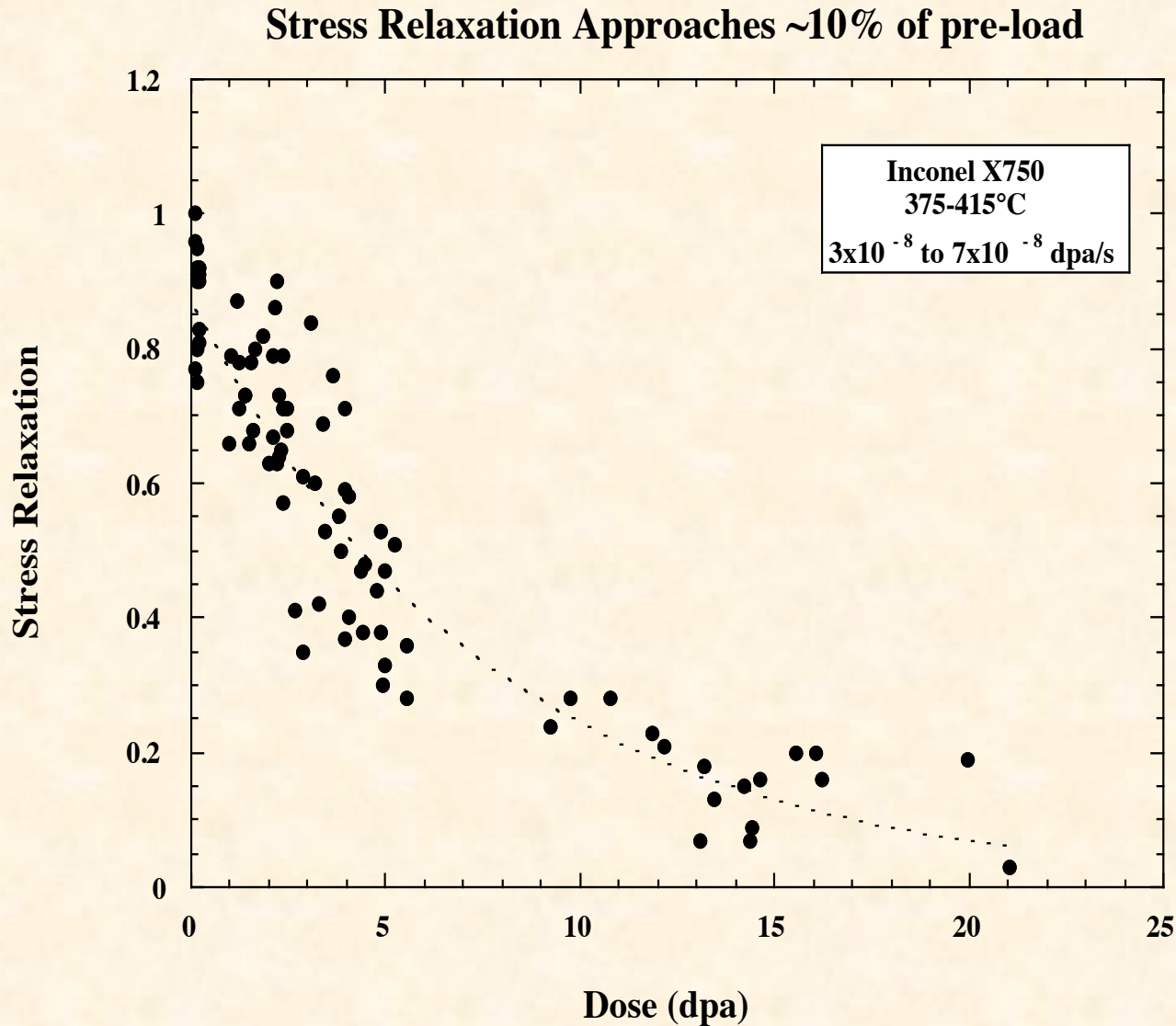
**Growth is preferential in Zr-alloys in basal plane directions.**



# Growth-induced strains vary greatly depending on orientation



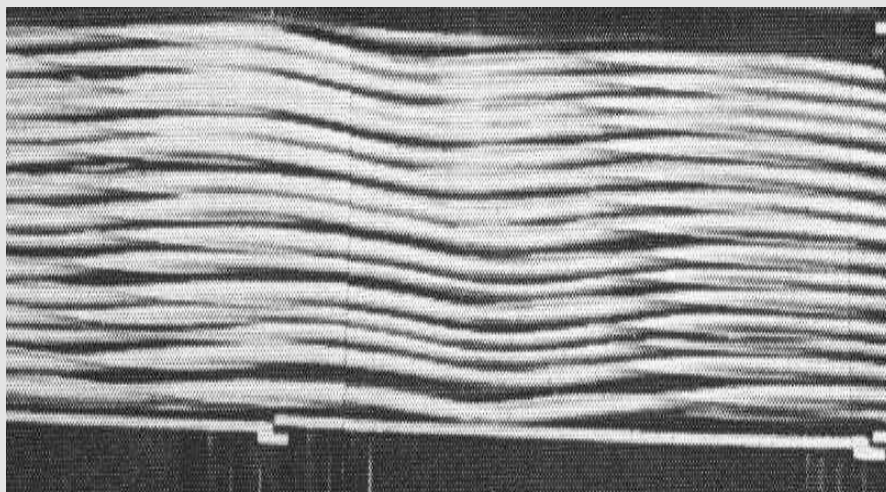
# Radiation-induced Stress Relaxation can be an issue for some components





# Swelling behavior under constrained conditions

- Swelling strains are isotropically distributed in the absence of constraint.
  - In presence of constraint the swelling strain is directed toward unconstrained or less-constrained directions.
  - Constraints can be externally applied or arise internally from gradients in swelling.
  - “Thick vs. Thin” data
- “Thin” implies no gradients in temperature, dpa rate or stress.



Stresses generated by swelling or swelling gradients will never exceed the yield stress.

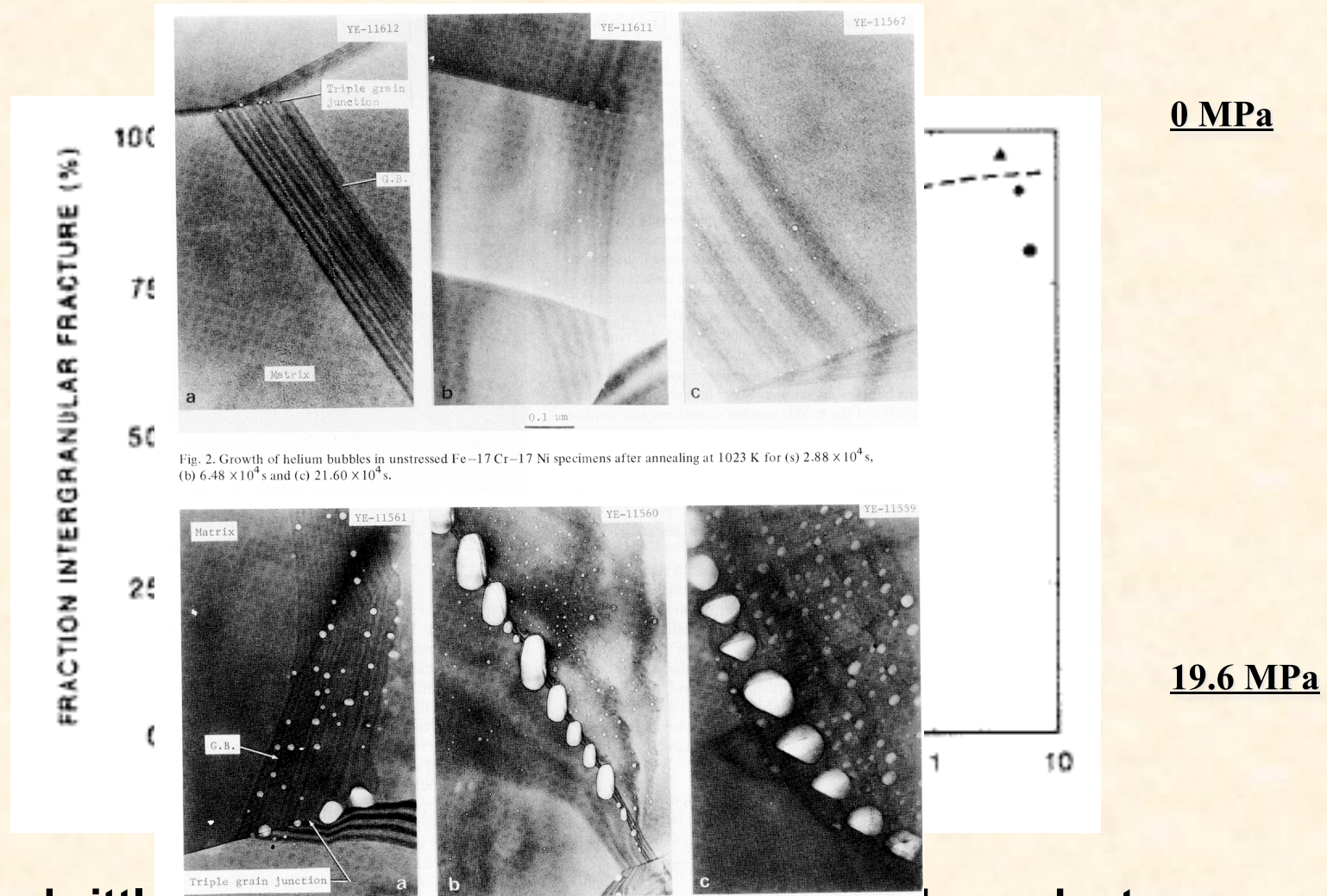
# Transmutation

- **Irradiation in a neutron environment can also result in transmutation.**
- **Transmutation products may influence materials properties.**
  - **Segregation**
  - **Precipitation**
  - **Chemical compatibility!**

# A number of common transmutation reactions in reactors can influence irradiation performance

- A number of important reactions occur in reactor environments, varying with spectrum and materials
- Most create helium
  - $^{58}\text{Ni} + n_f \rightarrow ^{55}\text{Fe} + ^4\text{He}$
  - $^{60}\text{Ni} + n_f \rightarrow ^{57}\text{Fe} + ^4\text{He}$
  - $^{58}\text{Ni} + n \rightarrow ^{59}\text{Ni} + \gamma \rightarrow ^{56}\text{Fe} + ^4\text{He}$
  - $^{10}\text{B} + n \rightarrow ^7\text{Li} + ^4\text{He}$
- He production is of interest due to implications on embrittlement in fast reactors.

# Helium Embrittlement for fast reactors



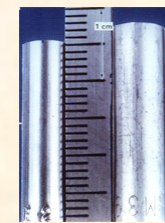
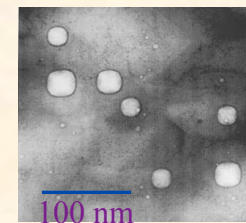
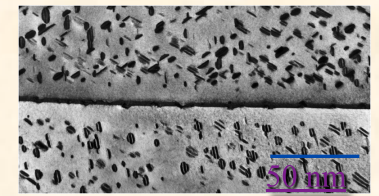
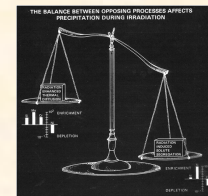
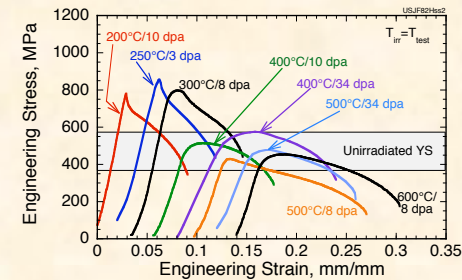
**Embrittlement via intergranular fracture is dependent on helium content, temperature, and strain rate**

van der Schaaf and Marshall, 1983



# Radiation Damage can Produce Large Changes in Structural Materials

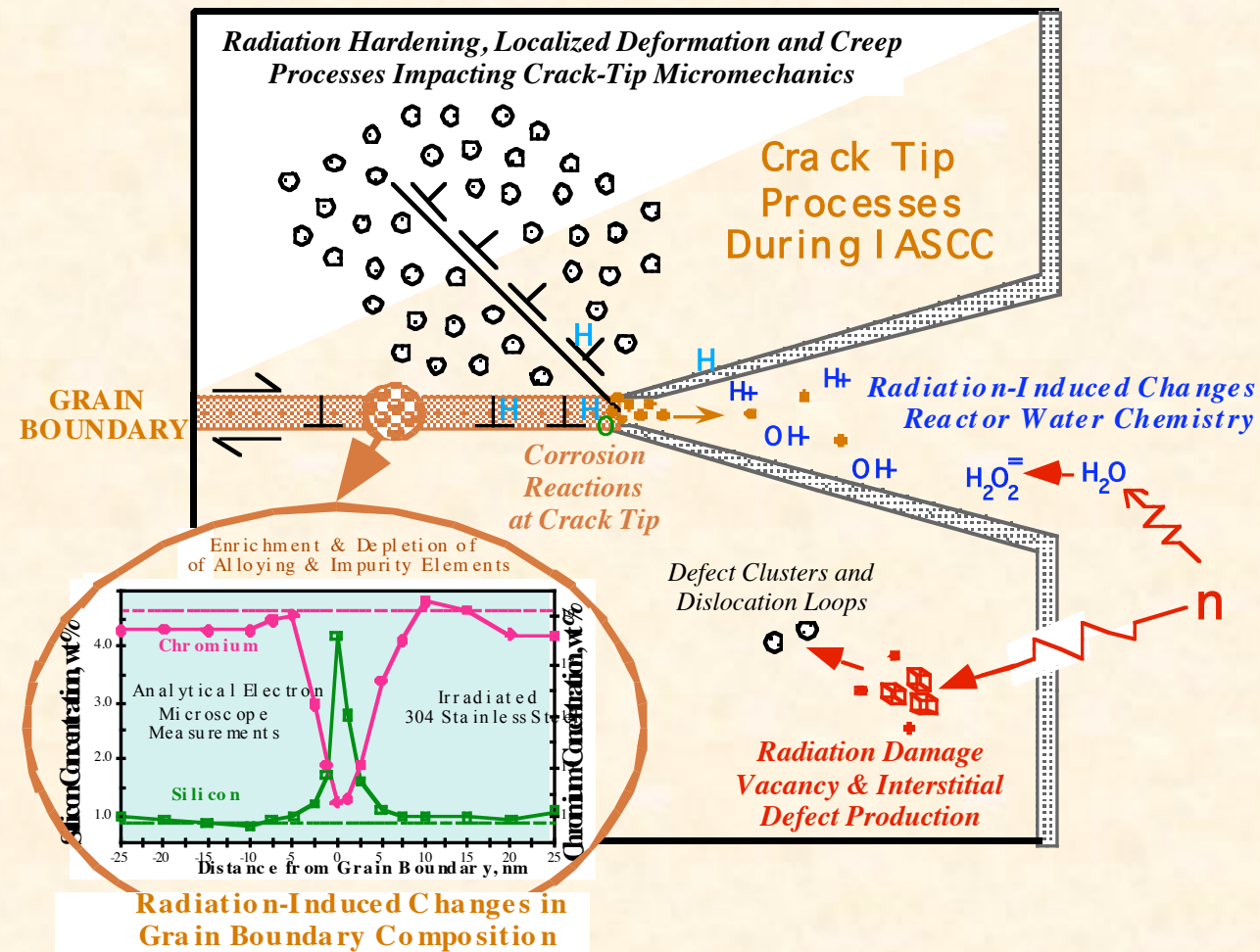
- **Radiation hardening and embrittlement** ( $<0.4 T_M$ ,  $>0.1$  dpa)
- **Phase instabilities from radiation-induced precipitation** ( $0.3-0.6 T_M$ ,  $>10$  dpa)
- **Irradiation creep** ( $<0.45 T_M$ ,  $>10$  dpa)
- **Volumetric swelling from void formation** ( $0.3-0.6 T_M$ ,  $>10$  dpa)
- **High temperature He embrittlement** ( $>0.5 T_M$ ,  $>10$  dpa)



Source: S. Zinkle



# Effects of Irradiation also influence corrosion processes



# Summary

- **All forms of irradiation damage are related to the creation and elimination of excess vacancies and interstitials.**
- **The interactions between these vacancies and interstitials determine the dominant form of irradiation-induced degradation.**
- **Many factors are important (temperature, dose, dose rate, alloy condition, alloy, stress and stress state).**
- **In LWR's, several forms of degradation are observed (RIS, RIP, hardening, embrittlement, swelling and creep)**
- **Other forms of degradation occur in other reactor applications.**

# **Thanks to the following for allowing me to use their slides!**

- **Gary Was**
- **Todd Allen**
- **Randy Nanstad**
- **Steve Zinkle**
- **Everett Bloom**
- **Steve Bruemmer**
- **Frank Garner**
- **Roger Stoller**
- **Lance Snead**